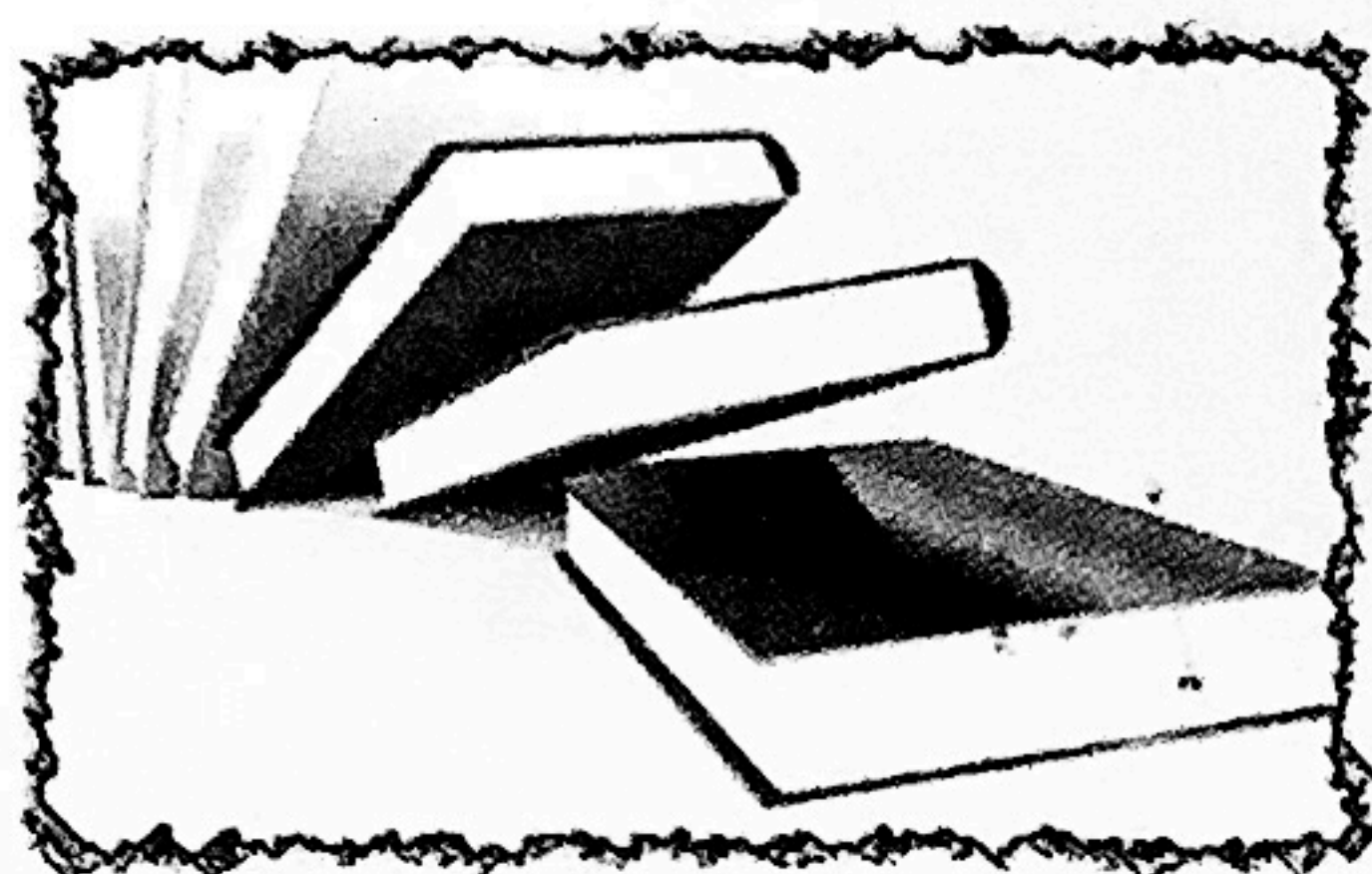


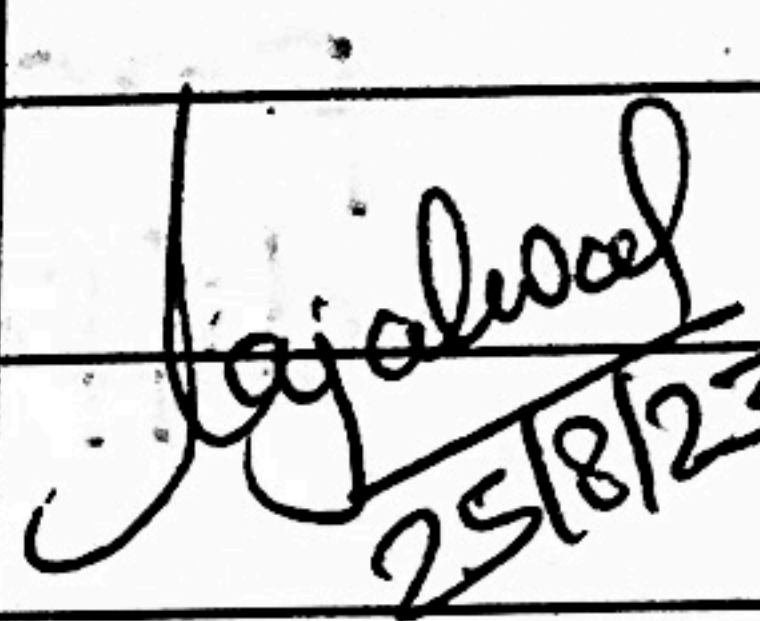
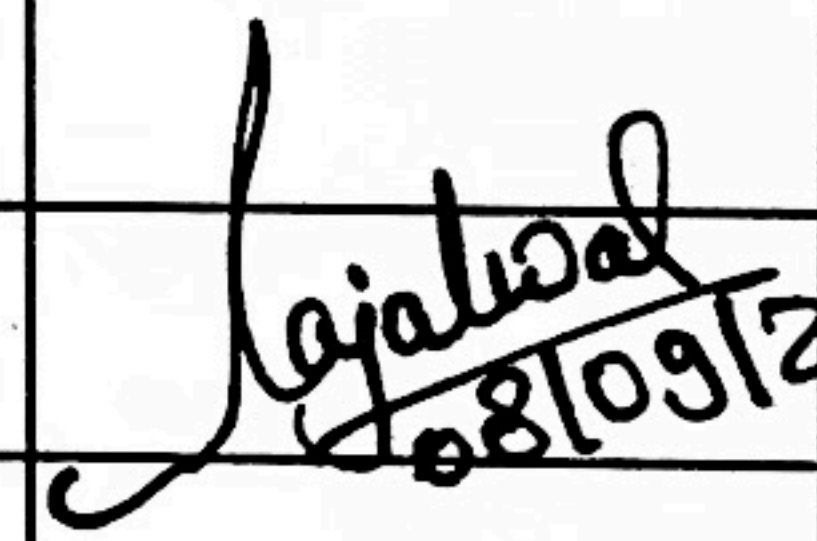

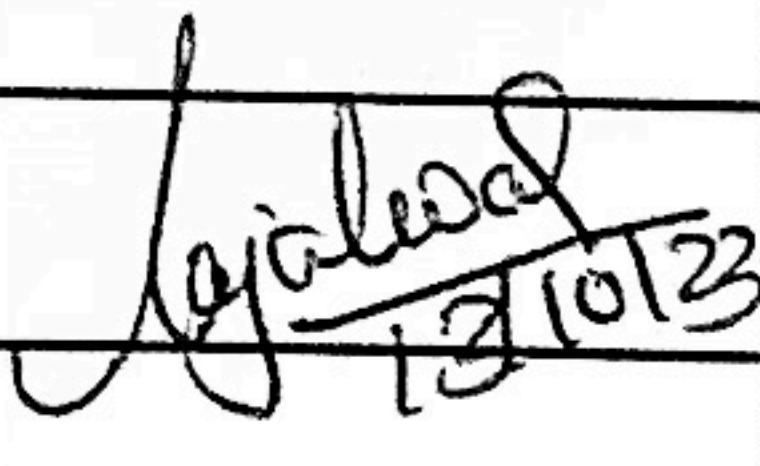
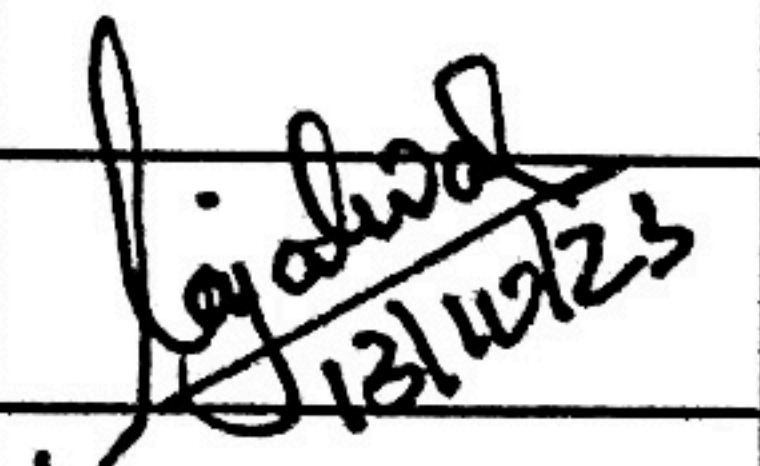
# I N D E X



Name DEBADATTA THAKUR

Class B.Tech Section EEE Roll No. 81 Year MO/23

Subject PS LAB (FRIDAY)

Sl. No.	Experiment Description	Experiment Date	Submission Date	Remarks Signature
1.	Ferro-Resonance characteristics.	11/08	18/08	 25/8/23
2.	Negative Sequence Reactance.	18/08	25/08	
3.	Over-Current Relay Characteristics.	25/08	1/09	
4.	Parallel Operations of AC Alternators.	1/9	8/9	 08/09/23
5.	Transformer Oil Breakdown Test.	8/9	15/9	 06/10/23
6.	Power Factor Control (L-load).	6/10	13/10	 13/10/23
7.	IDMT & DMT OC Relay characteristics (OC Relay).	6/10	13/10	 13/10/23



[illegible]



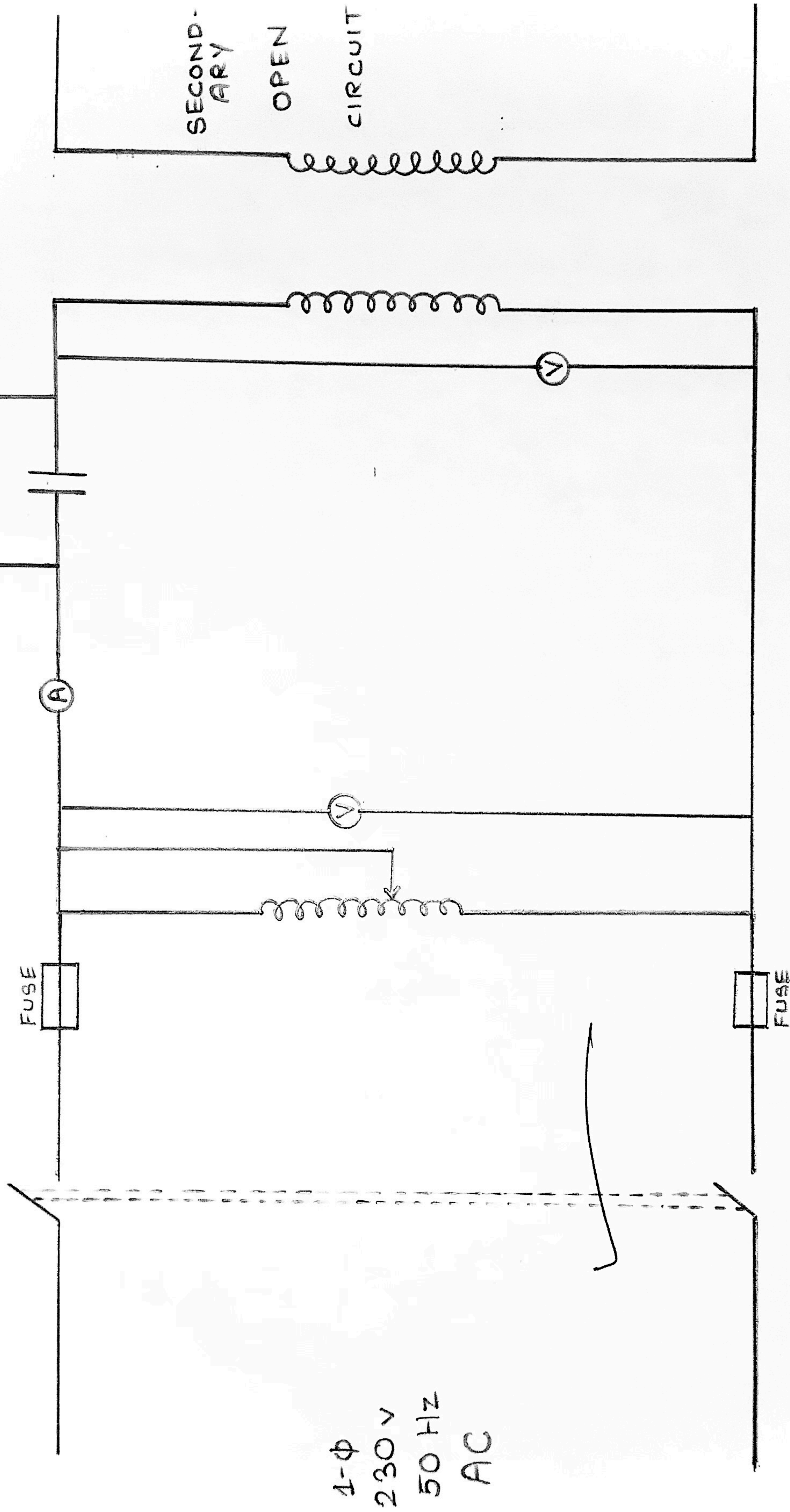


FIG 1.1

(CIRCUIT DIAGRAM)



## Experiment - 1

AIM - Obtain Ferro-Resonance characteristics of a 1- $\phi$  transformer at no-load.

### APPARATUS -

Capacitor ( $20 \mu F$ ), 1 nos.

1- $\phi$  Variac (230 V, 3 KVA), 1 nos.

1- $\phi$  Transformer (220/110 V), 1 nos.

AC Voltmeter (0-600 V), 1 nos.

AC Voltmeter (0-300 V), 1 nos.

AC Ammeter (0-10 A), 1 nos.

### THEORY -

Partial resonance condition occurs in power system when unbalanced configuration occurs so as to place capacitances in series with inductances. When a transformer is connected to a long transmission line and both are switched together, such a condition might occur.

The ferro-resonance occurs in a ferromagnetic material like the iron. If in a power system a cable is connected to a



# (CONDITIONS LEADING TO FERRO-RESONANCE)

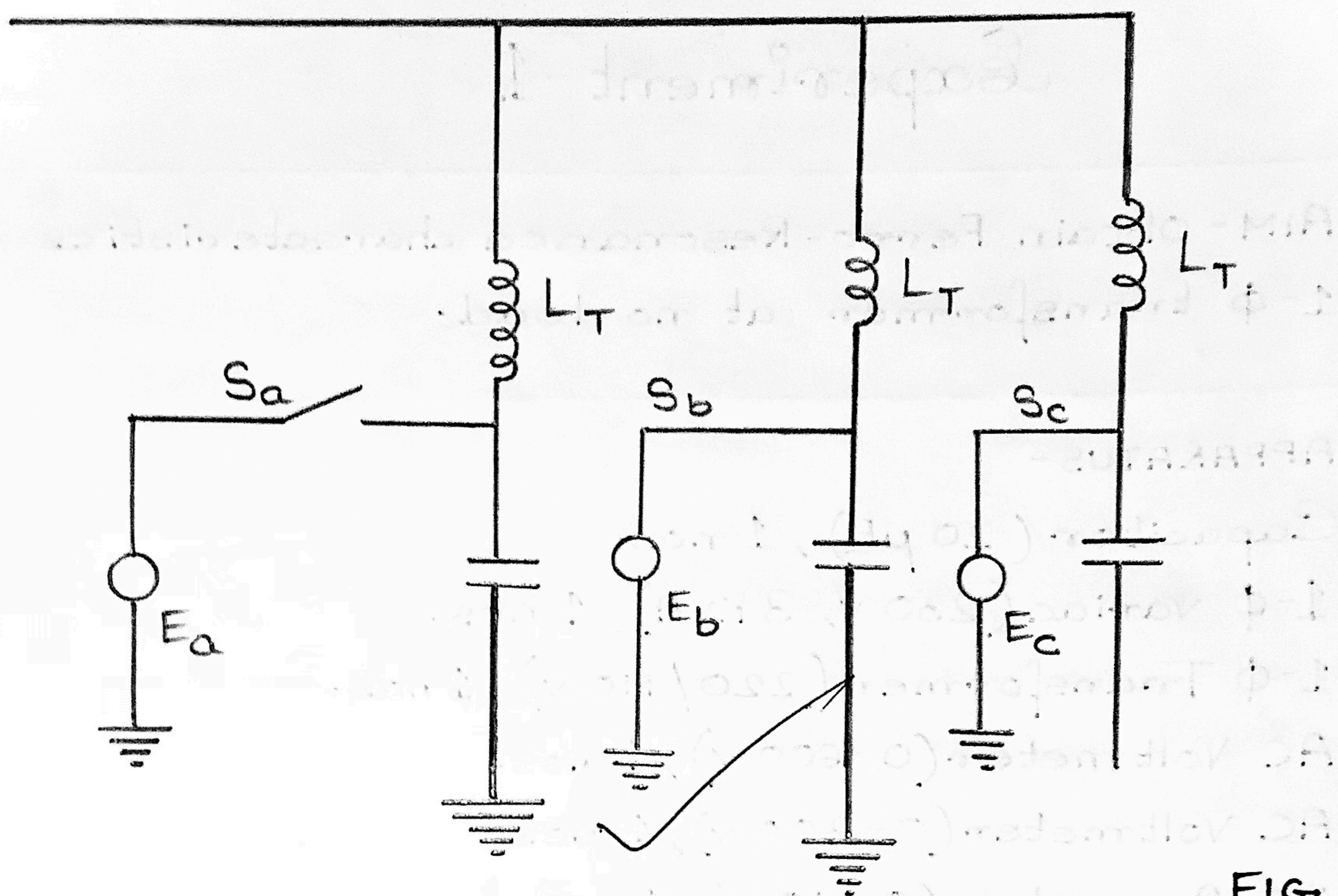


FIG 1.2

## (Generator connected to transformer)

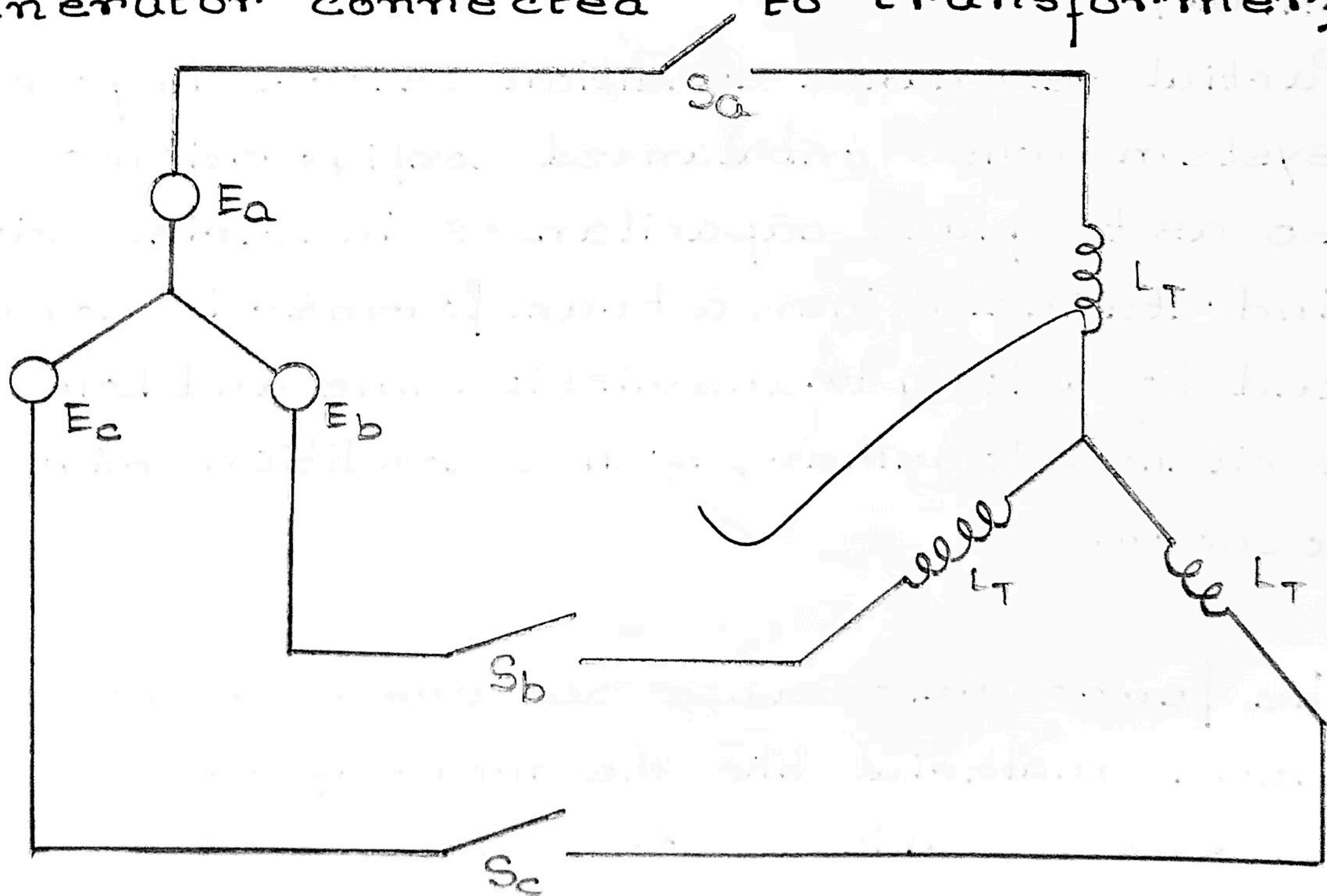


FIG 1.3



transformer winding acts as an inductor, the cable capacitance forms capacitor of the LC circuit.

### PROCEDURE-

Give AC voltage slowly via 1- $\phi$  variac. At one position there will be a sudden jump in voltage across capacitor & inductor. Now decrease voltage to zero supply and again there is a sudden fall in voltage. Plot  $V_1$  (supply voltage) and  $V_3$  (transformer voltage).

### OBSERVATION TABLE-

Sl.	$V_1$	$V_2$	$V_3$	A (amps)
1.	100	20	60	0.9
2.	140	20	85	1
3.	160	30	100	1.2
4.	177	250	170	4.5
5.	160	245	168	4.2
6.	140	230	163	4
7.	100	210	162	3.5
8.	60	15	40	1
9.	6	8	0.5	0.3



## Experiment-2

AIM - Determination of negative sequence reactance of a 3- $\phi$  alternator.

### APPARATUS -

1- $\phi$  Auto-Transformer (230 v, 3 KVA), 1 nos.

Rheostat (200  $\Omega$ , 2.8 A), 1 nos.

AC Voltmeter (0-600 v), 1 nos.

AC Ammeter (0-10 A), 1 nos.

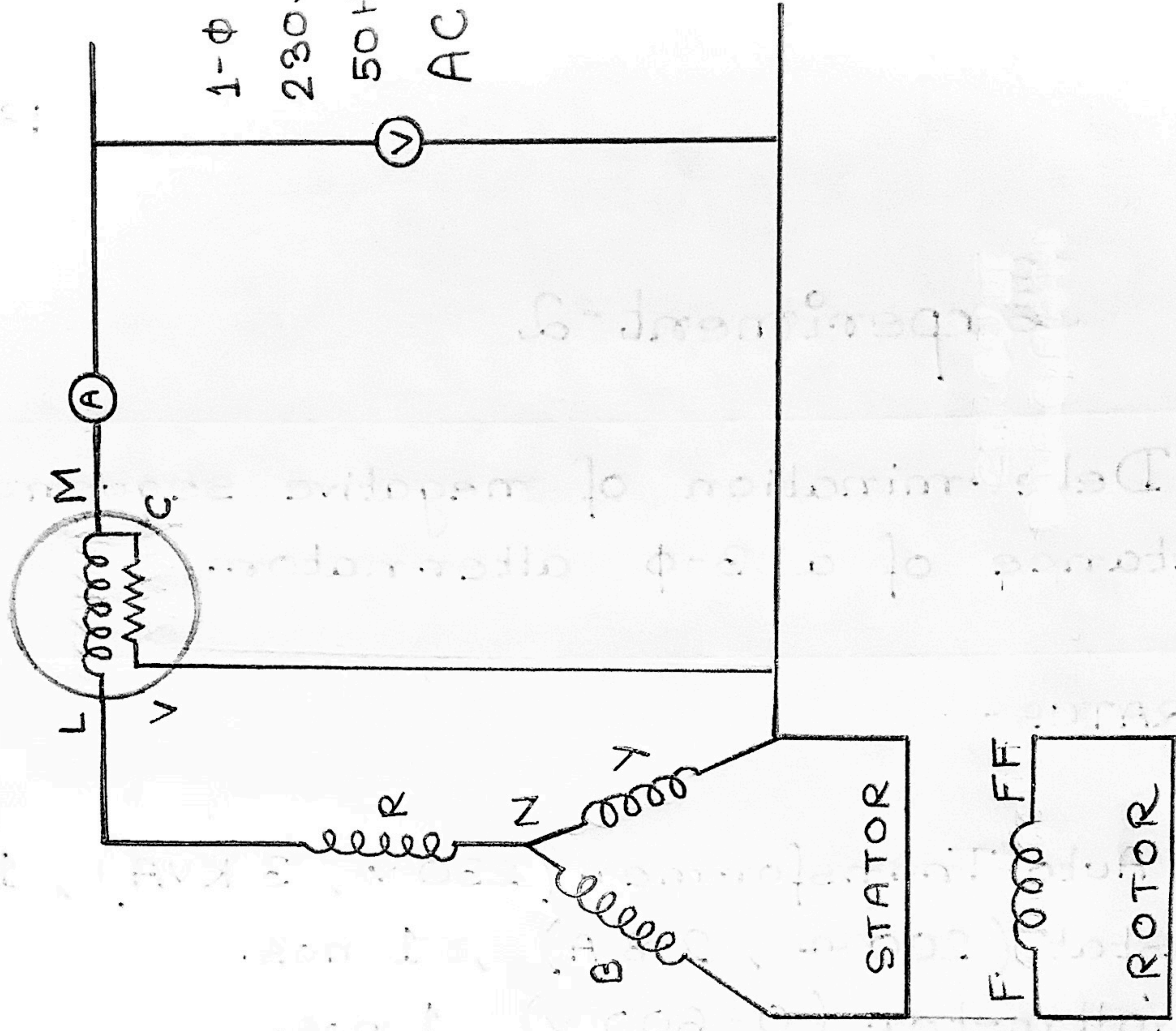
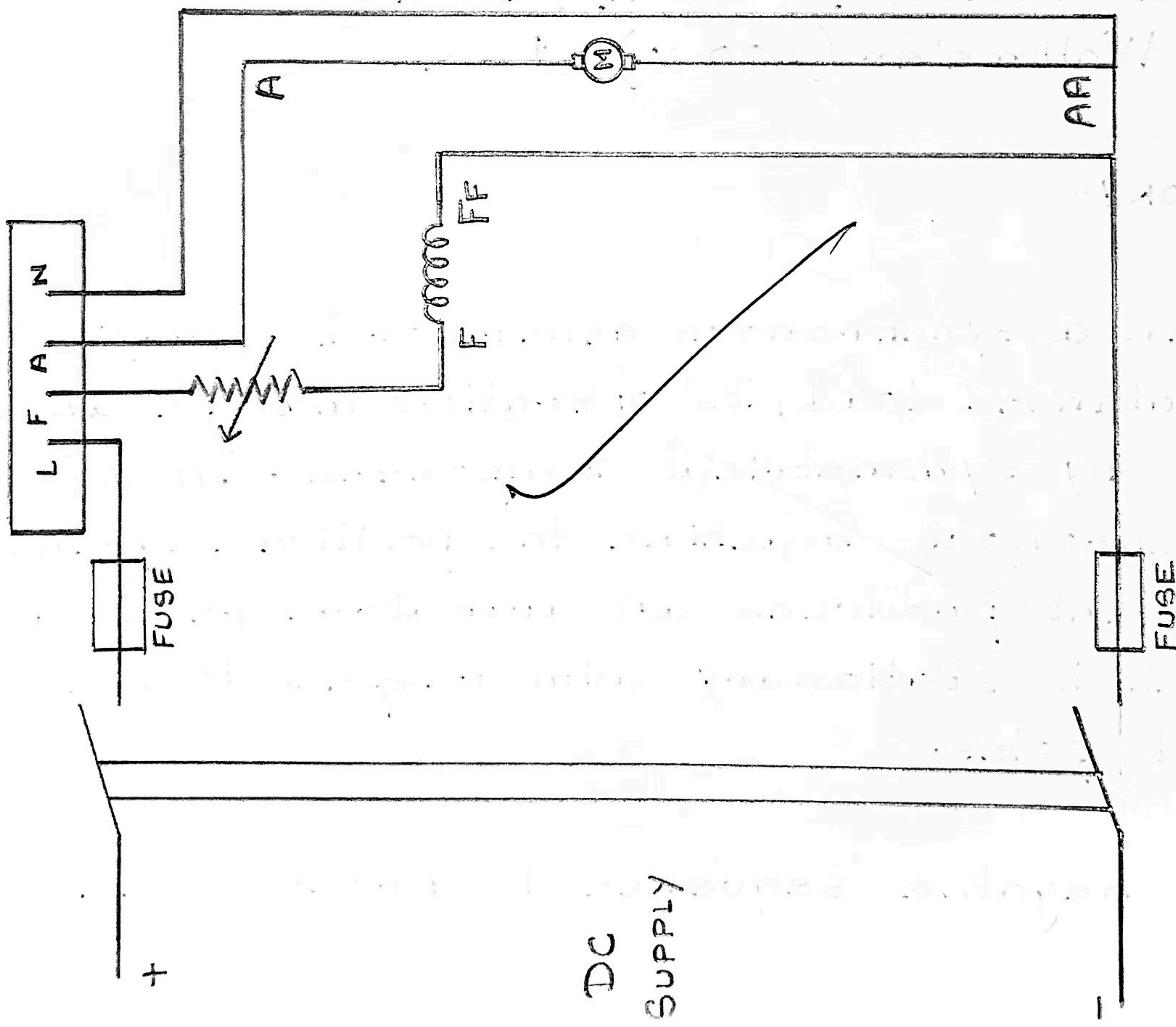
AC Wattmeter (600 v), 1 nos.

### THEORY -

When a synchronous generator is carrying an unbalanced load, its operation may be analysed by symmetrical components. In a synchronous machine the positive sequence current produces an armature reaction which is stationary with respect to the field poles.

The negative sequence is produced by an





CIRCUIT DIAGRAM



armature reaction which rotates around armature at synchronous speed in the direction to that of field poles at synchronous speed. Inducing current in the field damper winding and rotor iron. The impedance encountered by the -ve sequence is the -ve sequence impedance of the generator.

#### MATHEMATICAL FORMULAS -

$$V/I = Z_{eq} = 3/2 Z \therefore Z_{eq} = V/I$$

$$W = I^2 R_{eq} = I^2 \frac{3}{2} R \therefore R_{eq} = W/I^2$$

$$X = \sqrt{Z^2 - R^2}$$

$$R = \cancel{W} \text{ per phase} / I_{sc}^2 \therefore R = \frac{2}{3} R_{eq}$$

$$Z = 2V/3I \therefore Z = \frac{2}{3} Z_{eq}$$



## PROCEDURE -

a. Make connections and run DC motor at the synchronous speed while keeping the short circuit current low.

b. Apply 1- $\phi$  voltage and note readings.

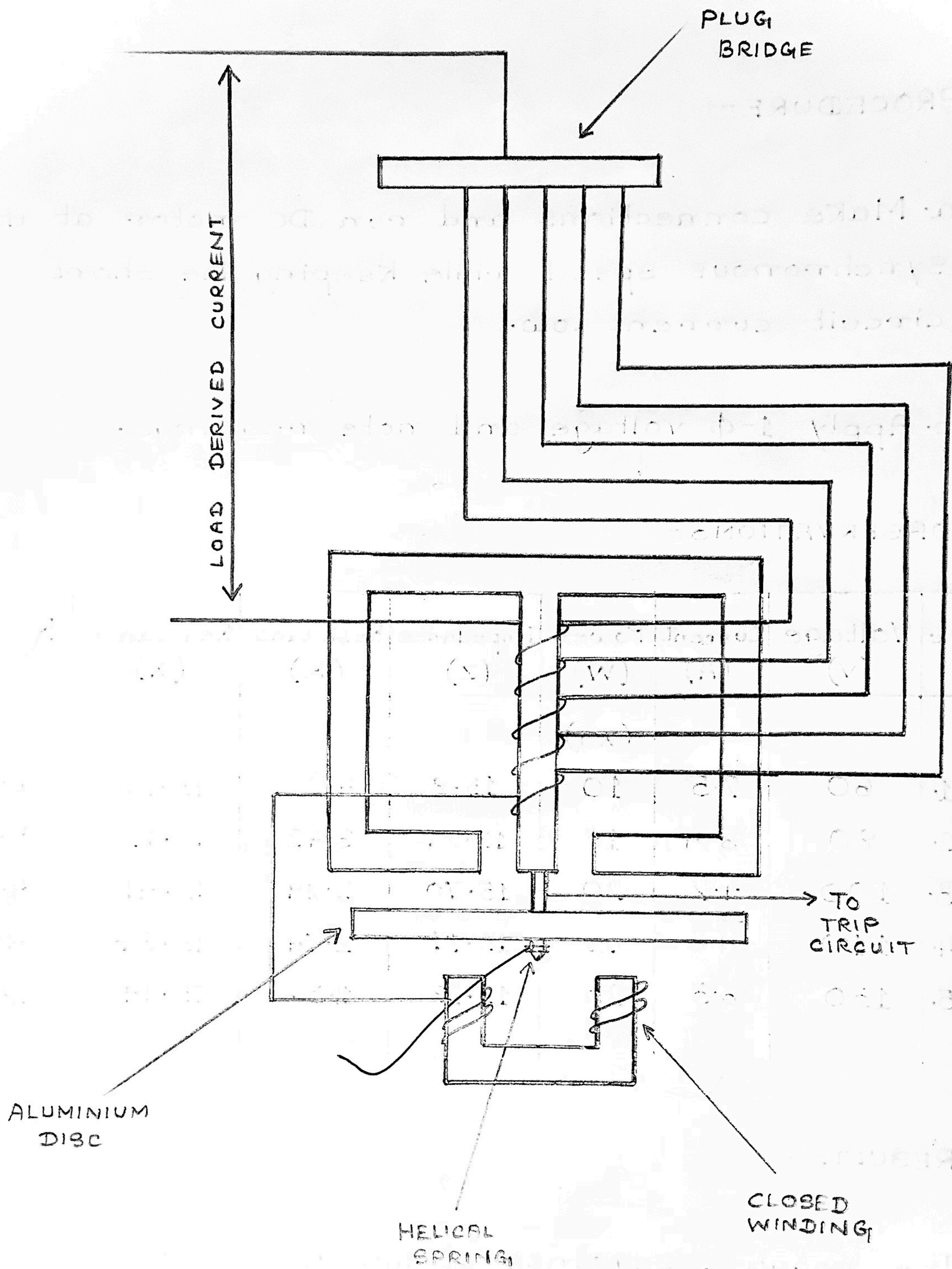
## OBSERVATIONS -

Sl.	Voltage (V)	Current (A)	Power (W)	Impedance (Z)	Resistance (R)	Reactance (X)	$R_{eq}$
			(x4)				
1.	60	2.5	10	15.8	4.22	15.26	6.40
2.	80	3.4	15	15.57	3.42	15.12	5.19
3.	100	4.2	20	15.70	2.99	15.41	4.53
4.	110	4.6	22	15.77	2.74	15.53	4.15
5.	150	6.5	25	15.23	1.56	15.14	2.36

## RESULTS -

The negative sequence of the alternator is found and it is  $X = 15.292 \Omega$





— OVER - CURRENT Relay



## Experiment-3

AIM - Determination of over-current relay characteristics using relay test setup.

### APPARATUS -

Over-Current Relay  
Relay Test Setup

### THEORY -

A protective relay is a device which detects the fault and initiates the operation of the circuit breaker to isolate the defective element from the healthy circuit.

~~Instantaneous over-current Relay - No time delay is provided for the operation.~~

Inverse Time over-current Relay - Operating time reduces as the actuating quantity increase in magnitude.



Inverse definite minimum time relay -  
Operating Time is inversely proportional to the fault current.

Very Inverse Relay - Saturation of core occurs at a later stage.

#### FORMULAE -

$$\text{PSM} = \frac{\text{Primary Fault Current}}{\text{Relay current Settings} \times \text{Current Transformer Ratio}}$$

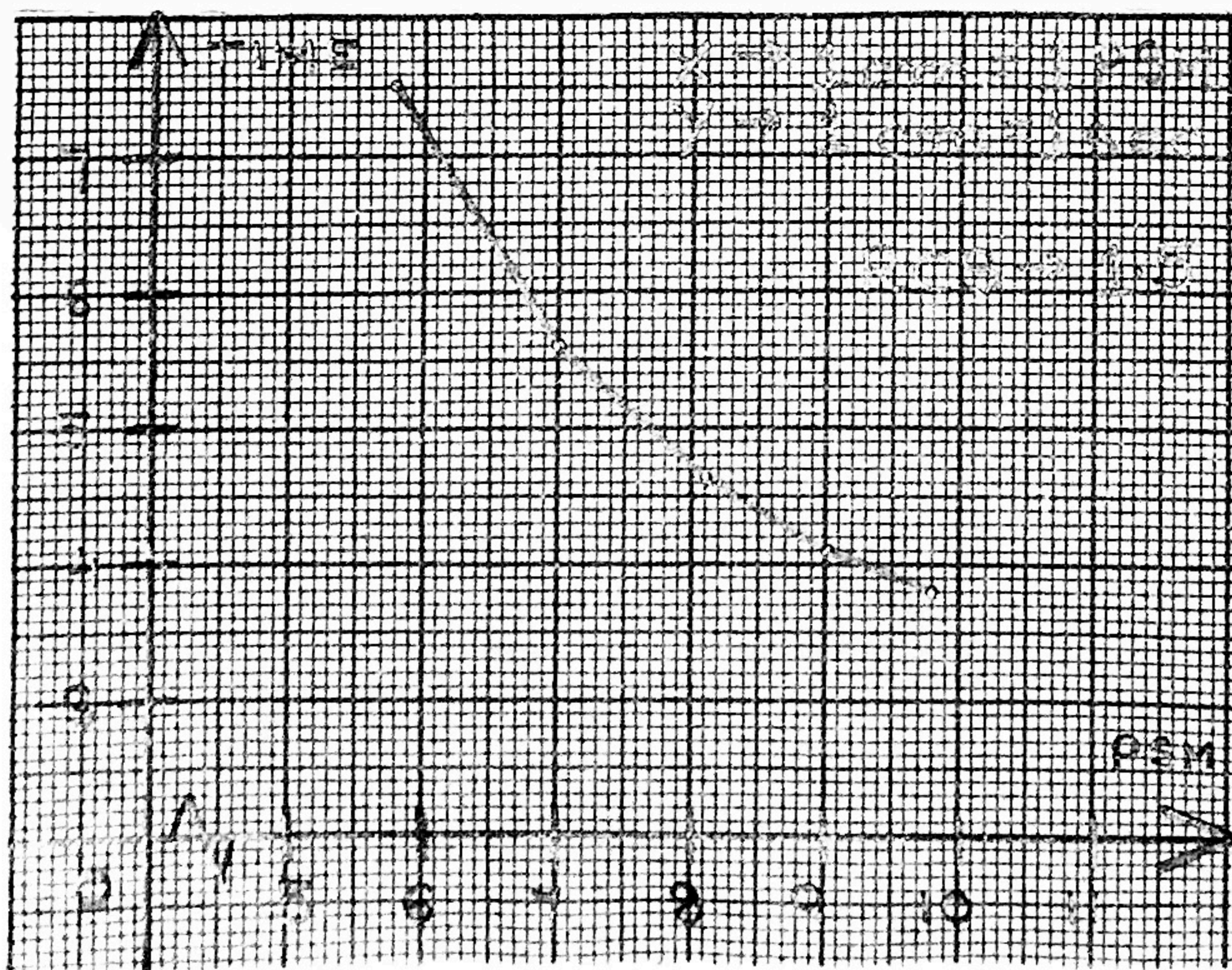
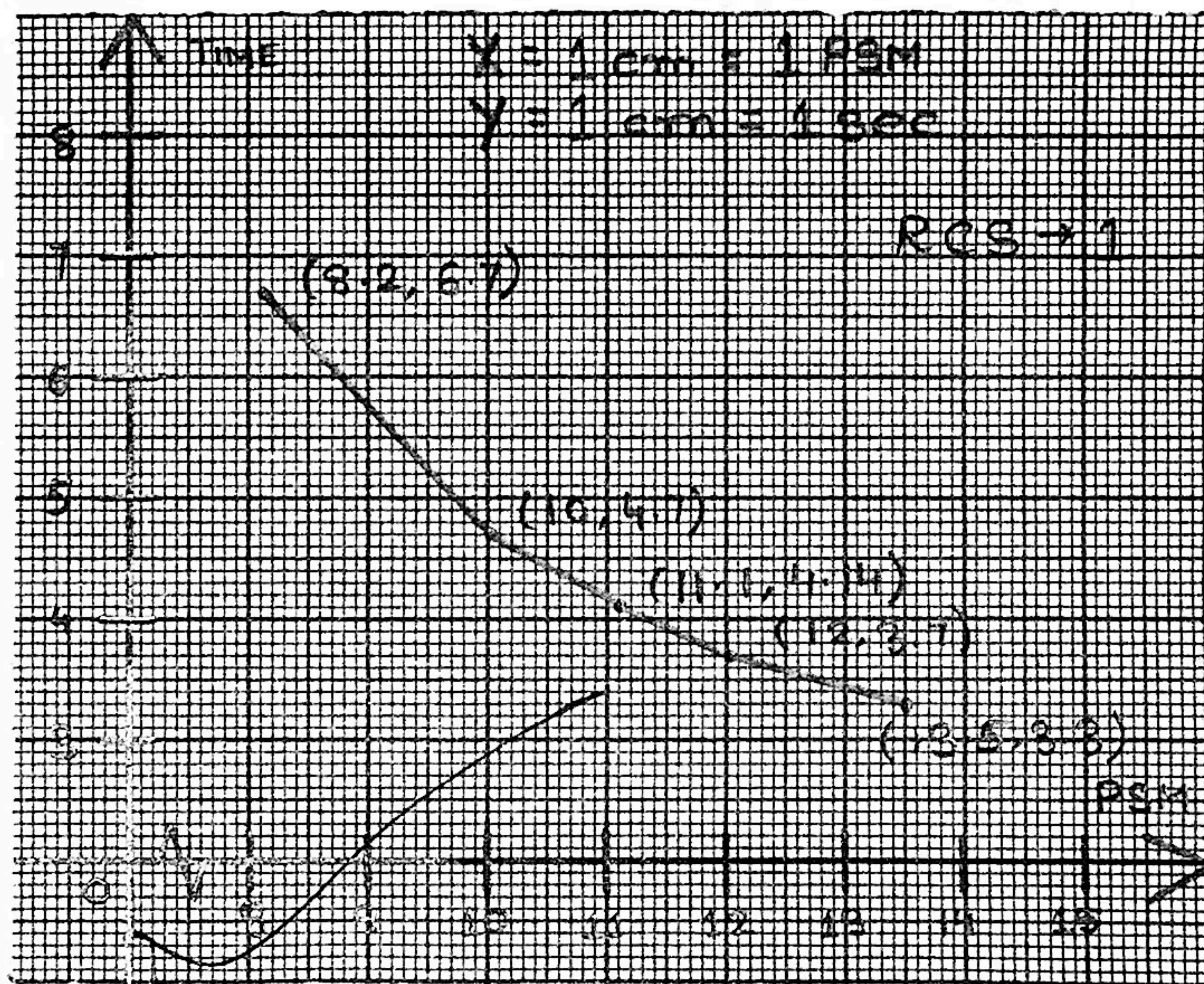
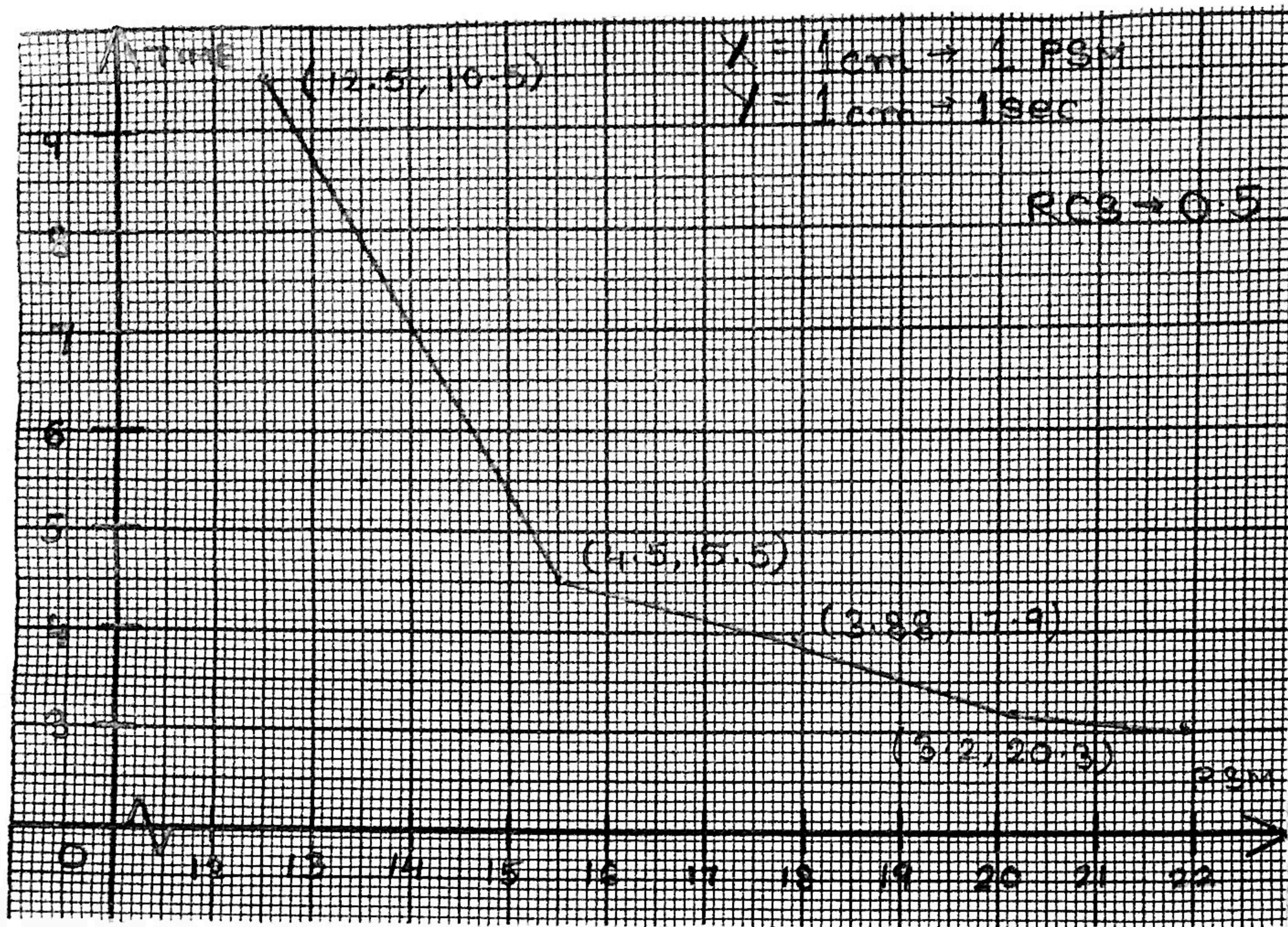
#### OBSERVATIONS -

Sl.	TIME	A%	A	P.S.M.
1.	10.5	25.2	6.26	12.52
2.	4.5	55.0	7.75	15.50
3.	3.88	79.2	8.96	17.92
4.	3.27	103.6	10.18	20.36
5.	3.01	118.1	10.90	21.80

Relay Current Setting  $\rightarrow 0.5$   
Ratio  $\rightarrow 1$

Teacher's Signature .....







SL.	TIME	A %	A	P.S.M.
1.	6.73	65.1	8.25	8.25
2.	4.76	101	10.05	10.05
3.	4.14	123.2	11.16	11.16
4.	3.79	140.6	12.03	12.03
5.	3.36	170.1	13.50	13.50

Relay Current Setting  $\rightarrow$  1

Ratio  $\rightarrow$  1

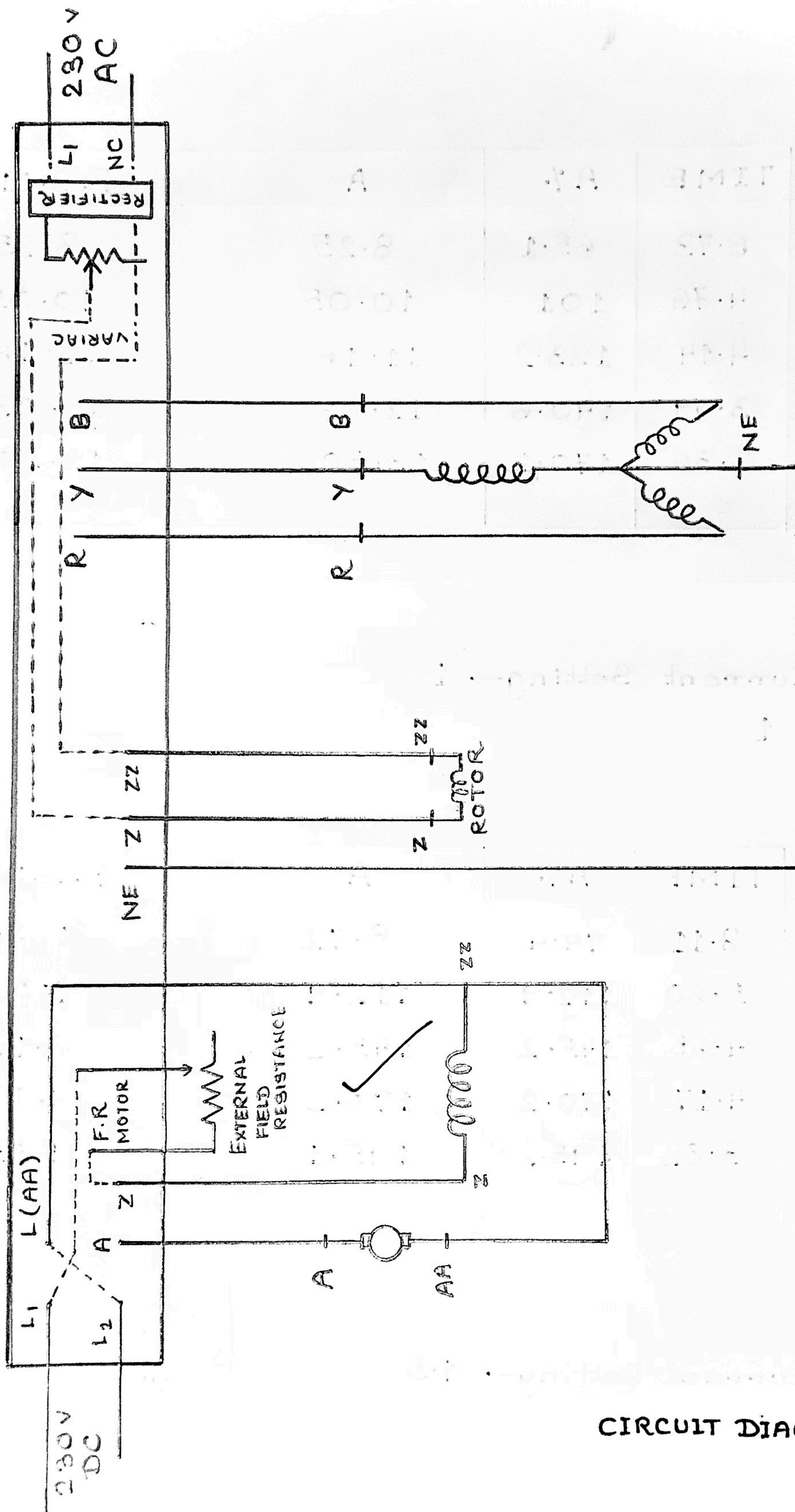
SL.	TIME	A %	A	P.S.M.
1.	8.11	74.4	8.72	5.81
2.	5.60	112.9	112.9	7.09
3.	4.65	145.2	145.2	8.17
4.	4.17	170.2	170.2	9.00
5.	3.82	195.2	195.1	9.83

Relay Current Setting  $\rightarrow$  1.5

Ratio  $\rightarrow$  1

*Lajal*  
01/09/23





CIRCUIT DIAGRAM - 1



## Experiment - 4

AIM - Study of Synchronizing panel for parallel operation of AC generator.

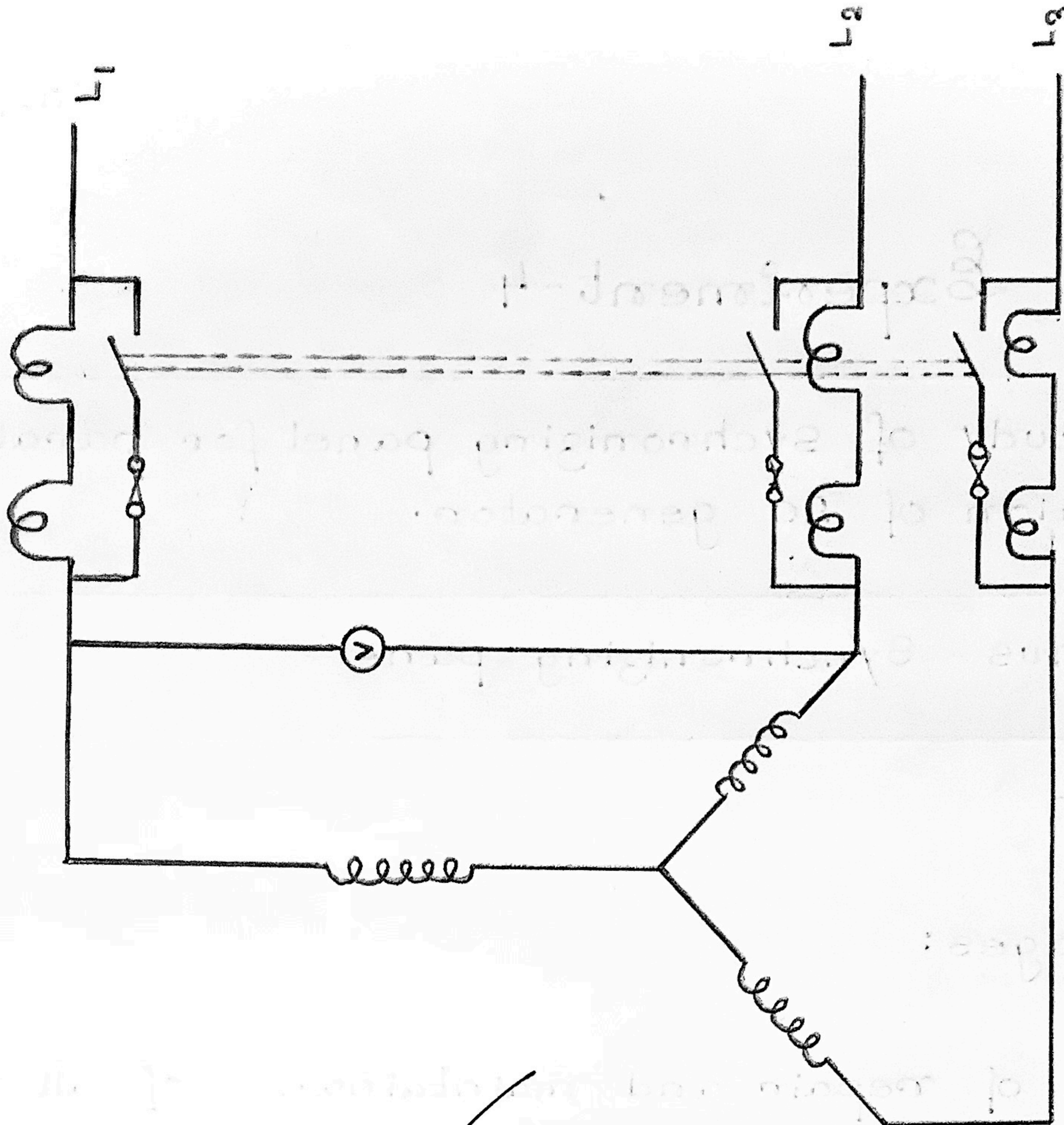
APPARATUS - Synchronizing panel

THEORY -

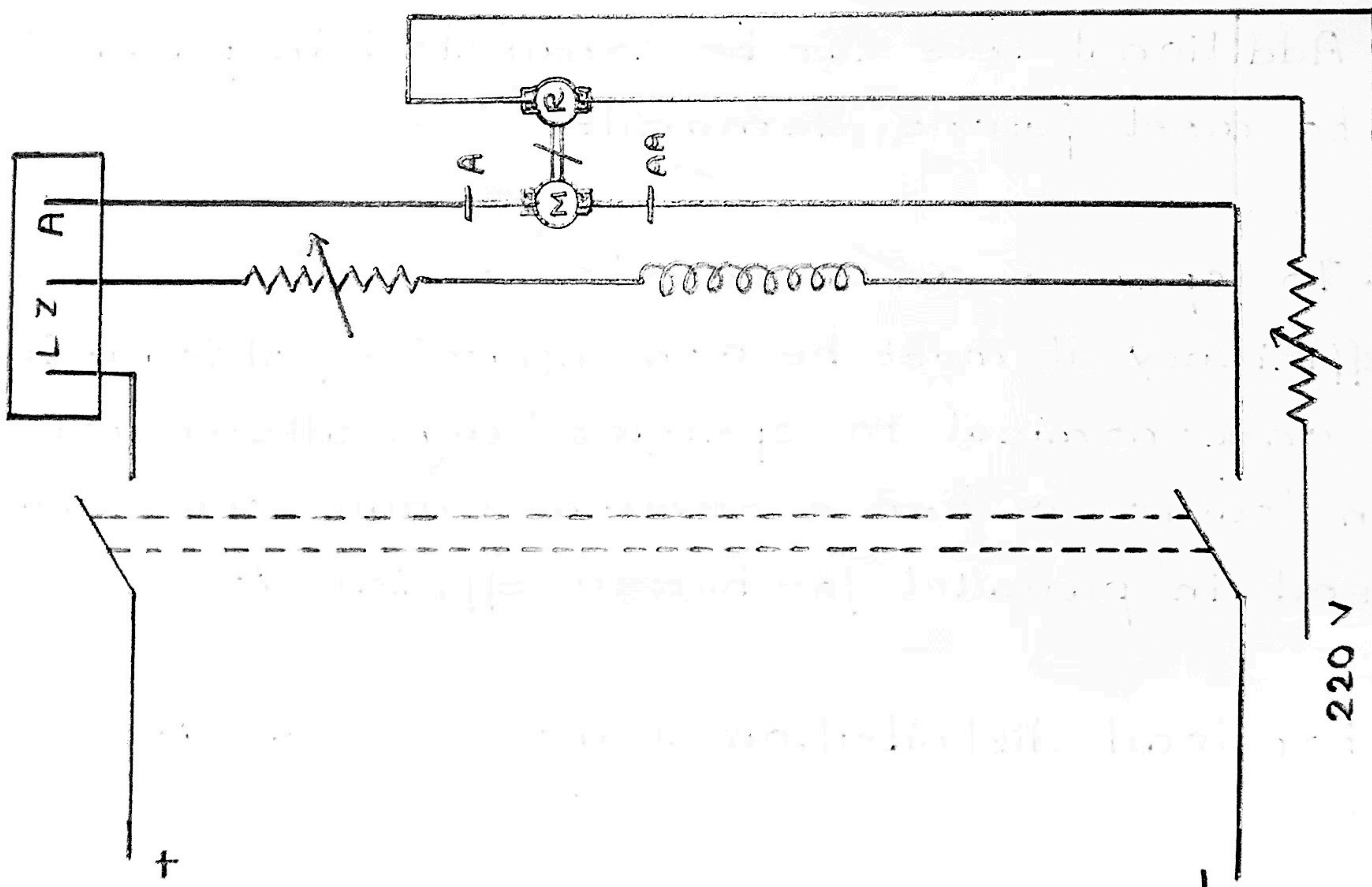
Advantages:

- a. Ease of repair and maintainance of all the individual units keeping continuity of supply.
- b. Additional sets can be connected in parallel to meet future demands.
- c. To operate an alternator on maximum efficiency it must be run near its full load. It is uneconomical to operate large alternators on low loads hence several small units are used in parallel for better efficiency.
- d. For load distribution & more reliability.





CIRCUIT  
DIAGRAM-2





### Conditions:

- a. The generated voltage of the incoming alternator to be connected in parallel with a bus-bar should be equal to bus bar voltage.
- b. Frequency of generated voltage of incoming alternator should be equal to bus-bar frequency.
- c. Phase sequence must be same.
- d. Phase difference must be same.

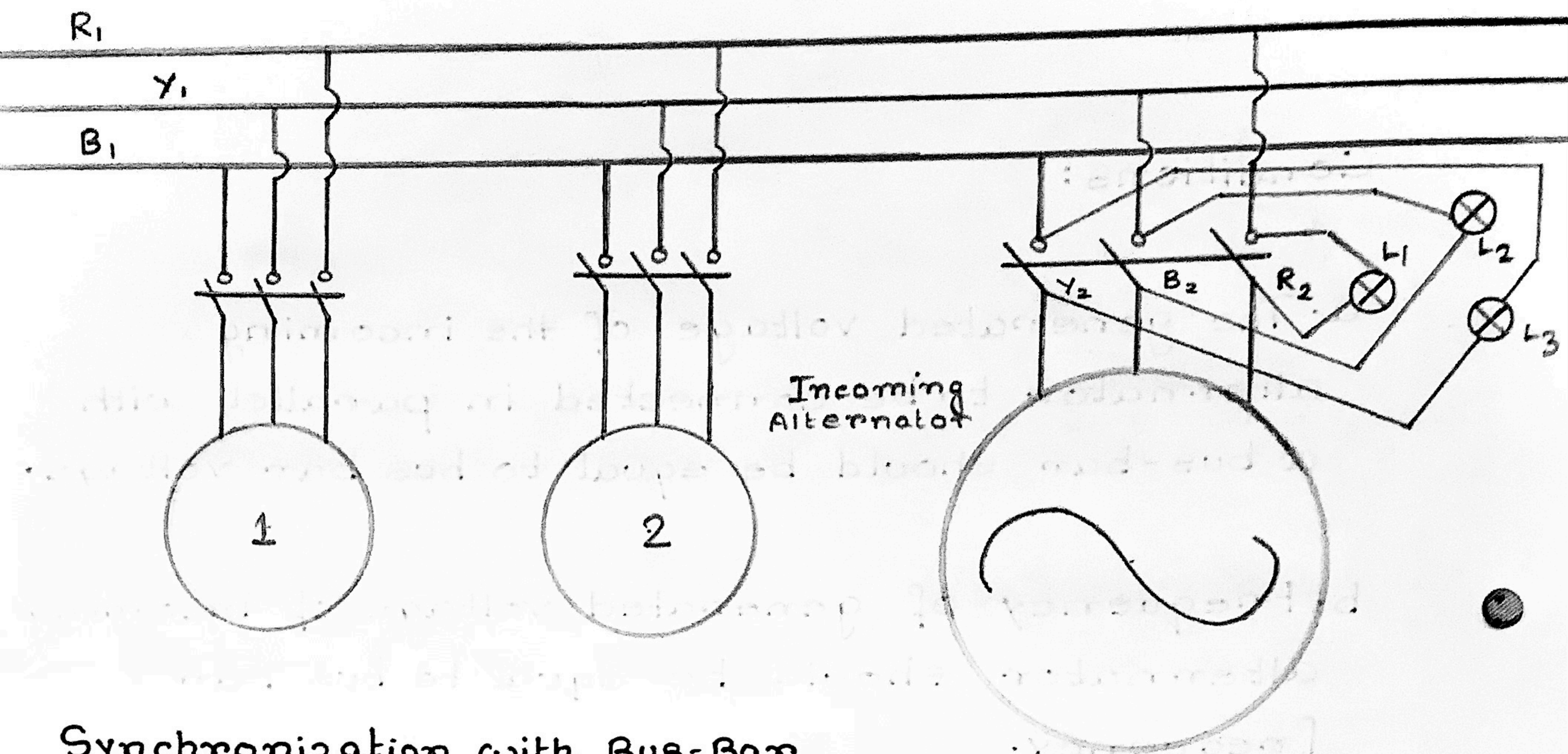
### Methods :

- a. Using THREE Lamps ✓
- b. Using a synchroscope

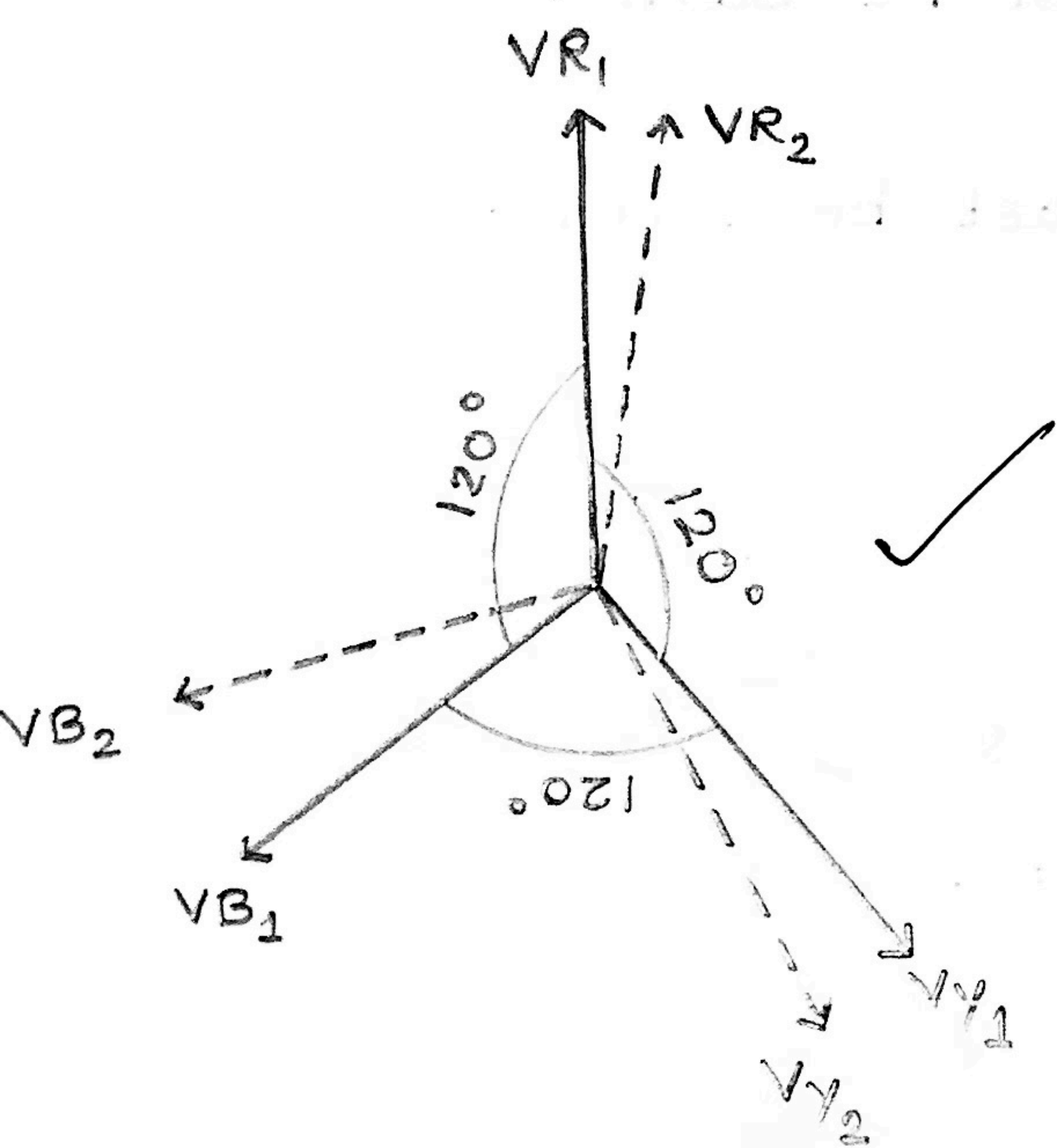
### PROCEDURE:

Make connections and ensure that the synchro-  
nising switch is open, external resistance  
in field circuit of motor is zero and

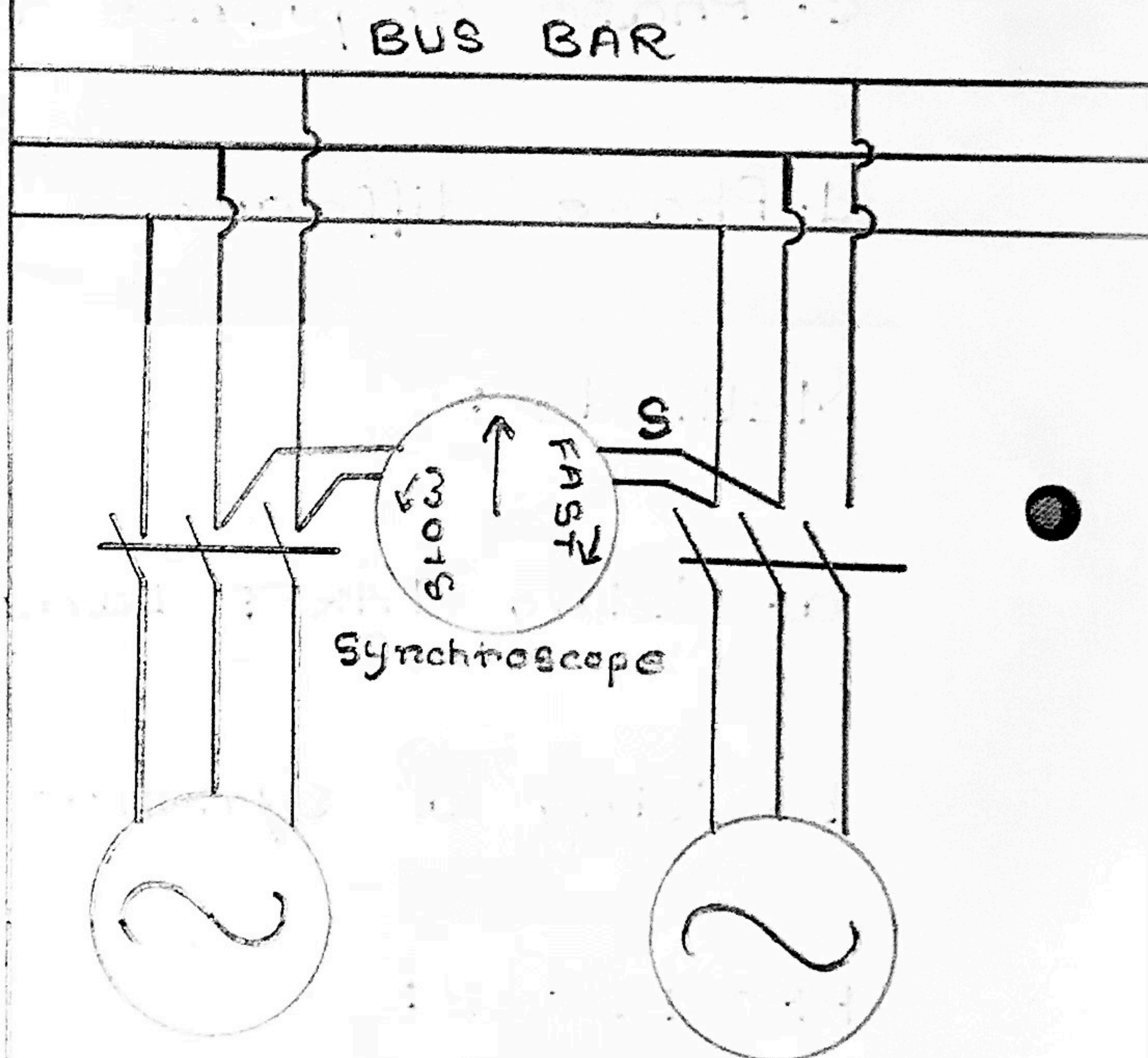




Synchronization with Bus-Bar



Same phase Sequence



Synchroscope Synchronization



of the alternator is maximum. Switch on DC motor-1 and 2 using Starter. Adjust their speed to rated speed of alternator. Switch on DC supply to field of alternator. Look out the Synchroscope and when it is exactly in middle close switch and once synchronized switch off synchronizing switch, bus-bar switch, DC mains & motor and alternator.

### PRECAUTIONS-

- a. Always switch ON DC motor after ensuring it is loaded only, the AC generator.
- b. MCB for synchroscope should be OFF.
- c. MCB for DC Excitor must be in OFF.

### RESULT-

AC generators were successfully synchronized using the synchronizing panel.

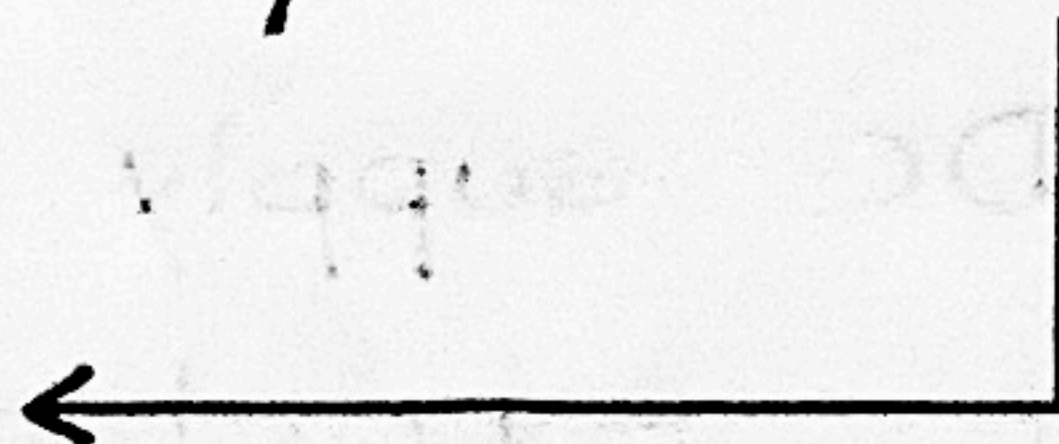
*Signature*  
08/09/23



SL.	kV(2.5mm)
1.	17
2.	27
3.	29
4.	24
5.	23
6.	29
7.	37
8.	31
9.	30



Breakdown Voltages  
for 2.5 mm gap



SL.	kV(2mm)
1.	35
2.	28
3.	35
4.	30
5.	33
6.	34



Breakdown Voltages  
for 2mm gap





## Experiment - 5

**AIM** - Determining breakdown voltage of the transformer oil using Kit.

**APPARATUS** - Transformer oil test Kit.

**THEORY** - The set is admirably suited for testing the dielectric strength of insulating oils. Samples are taken and the gap is adjusted and locked. It works on the same principle as high voltage test. A gap of 2 mm & 2.5 mm are tested. The must be filled to within a centimeter of the brim.

### PROCEDURE -

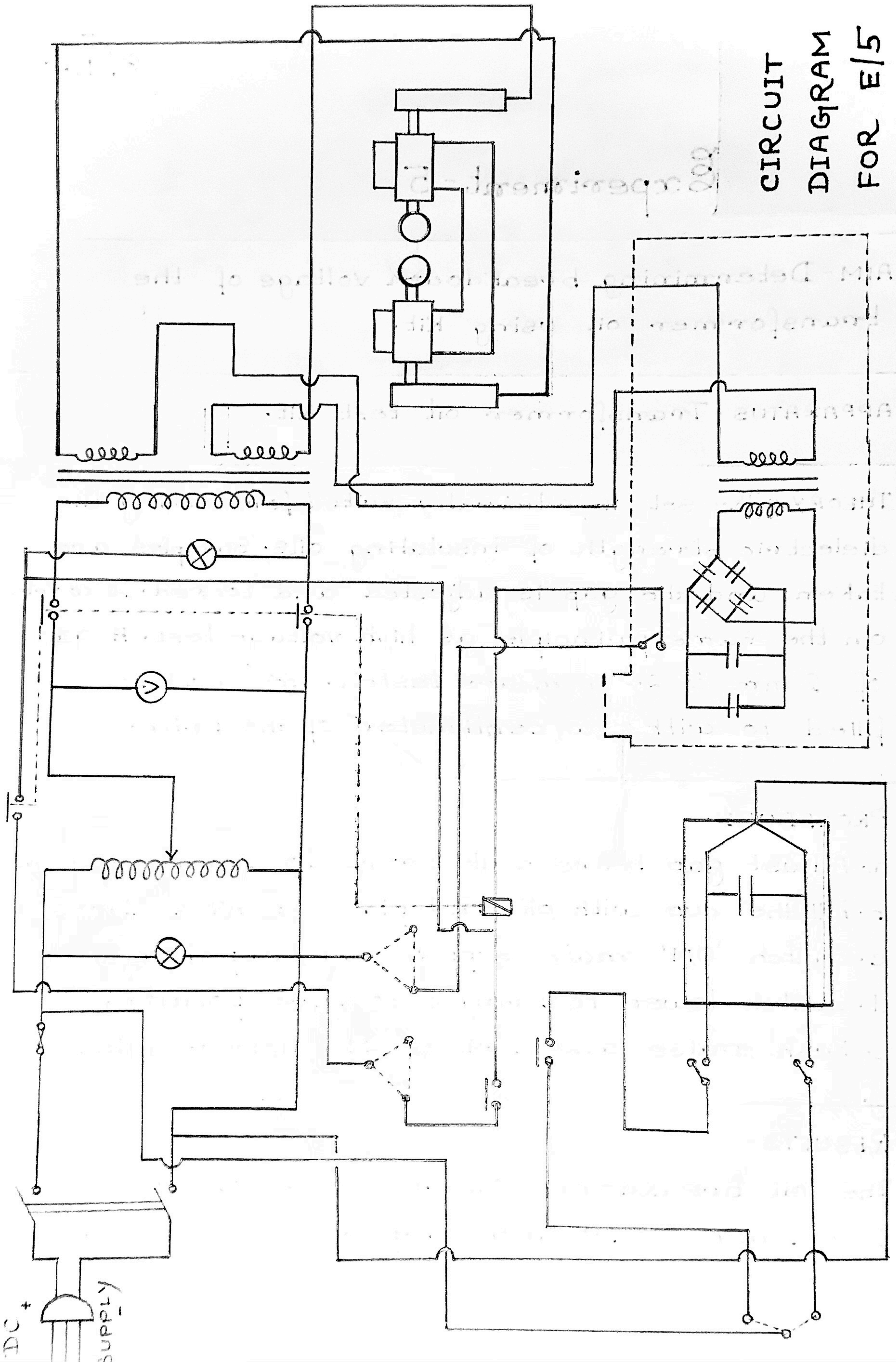
- Adjust gap between electrodes to 2 mm or 2.5 mm
- Fill the cup with oil and place on HT electrodes.
- Switch 'ON' main supply and lamp glows.
- Switch lower to bring it to zero position.
- Push raise and switch 'ON', note readings.

### RESULTS -

The oil breakdown voltages were observed for 2 mm & 2.5 mm gap in electrodes.



CIRCUIT  
DIAGRAM  
FOR E/5





### TECHNICAL SPECIFICATIONS:

Input : 230 v , 1- $\phi$  , 50 Hz AC

Output : 0-60 kV

Capacity : 1 kVA

### CONSTRUCTION :

All the components are involved in the compact & rugged device and are mounted on front VHT transformer. It is epoxy resist cast on which HT output terminals are provided on top plate. These HT electrodes are shaped suitably to accommodate the setup.

### PRECAUTIONS :

- The top lid must be pressed for setup to work.
- Transformer Oil must not be filled to the brim.
- Sudden high voltage must not be applied.

Jajawal  
6/10/23



## Experiment - 6

AIM - Power Factor control of an inductive load using power factor connection kit.

### APPARATUS -

Power Factor Correction Kit (1 no.)

Resistive Load (1 no.)

Connecting Wires

### THEORY -

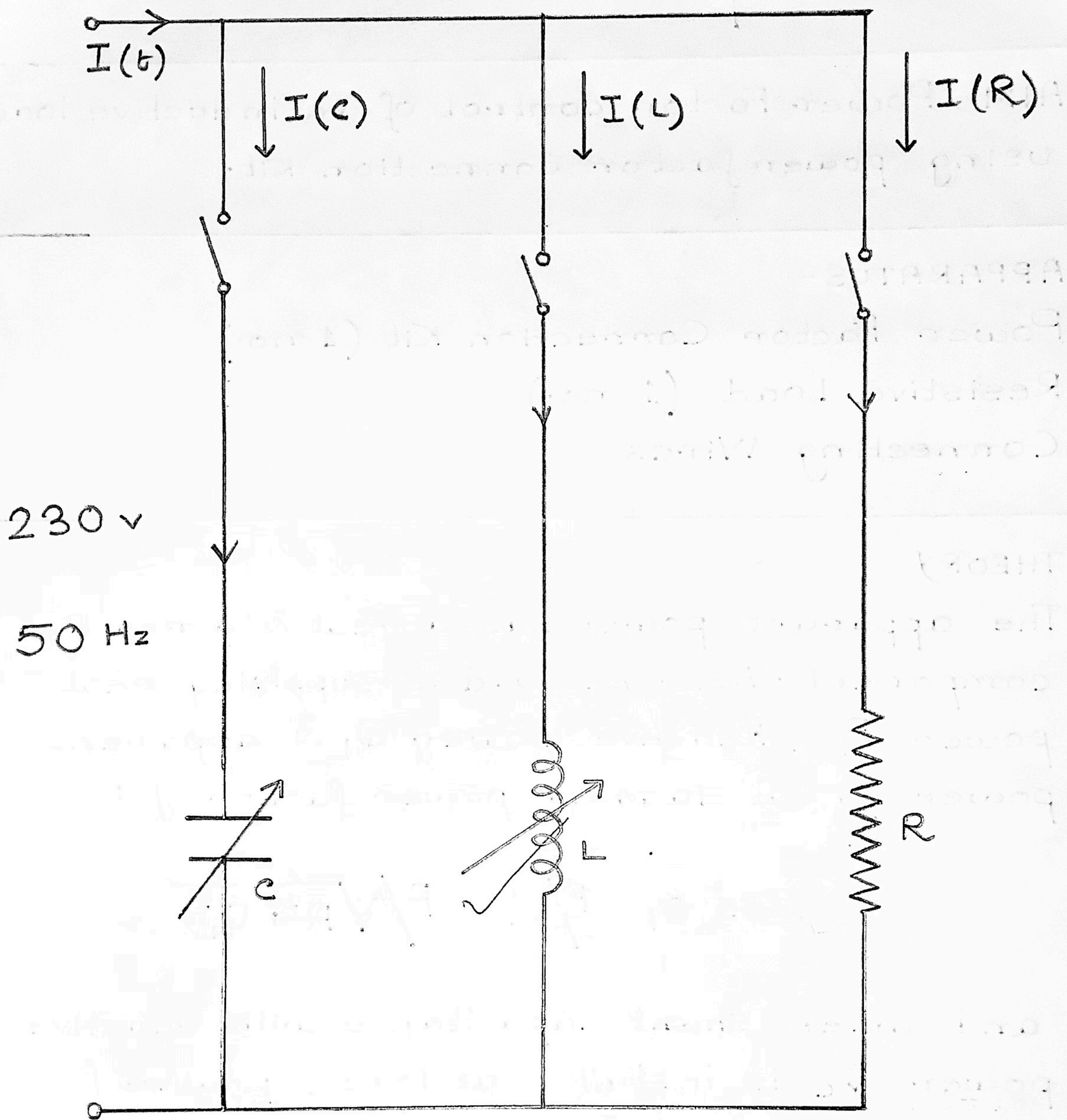
The apparant power has a real & a reactive component. Assume load is supplying real power  $P$ , Reactive power  $Q$ , & apparent power  $S$ , at lagging power factor of :

$$\cos \theta_1 = P/S_1 = P/\sqrt{P^2 + Q_1^2}$$

and when shunt capacitance with reactive power  $Q_c$  is installed at load, power factor can be improved from  $\cos \theta_1$  to  $\cos \theta_2$ .

$$\cos \theta_2 = P/S_2 = P/\sqrt{P^2 + (Q_1^2 - Q_2^2)}$$





CIRCUIT  
DIAGRAM  
FOR E/6



### PROCEDURE:

With a parallel connection of resistive and the inductive load switch on supply and vary the inductive load to have a power factor of 0.8 while noting  $I_T$ ,  $I_L$  &  $I_R$ .

Then switch on capacitor & increase value to have unity p.f. Then note  $I_T$ ,  $I_L$ ,  $I_R$  &  $I_C$ .

Repeat process.

### DISADVANTAGE OF LOW P.F.

1. Large KVA rating of machine
2. Greater Conductor Size.
3. High Copper loss.
4. Poor Voltage regulation

### PRECAUTIONS:

Take readings of power factor when selector switch is at individual position.

Take readings without parallel error.

### RESULT:

Power Factor of an inductive load was improved with the usage of a shunt capacitance.



**CALCULATIONS :**

$$1. \cos \theta_1 = 0.8, \theta_1 = \cos^{-1}(0.8)$$

$$\Rightarrow \theta_1 = 36.86$$

$$\therefore Q_1 = VI_T \sin \theta_1 = 230 \times 1.4 \times \sin 36.86$$

$$\Rightarrow Q_1 = 189.98$$

$$\text{Also } \cos \theta_2 = 0.98, \theta_2 = \cos^{-1}(0.98)$$

$$\Rightarrow \theta_2 = 11.47$$

$$\therefore Q_2 = 230 \times 1 \times \sin 11.47 = 45.54$$

$$\text{Hence } Q = Q_1 - Q_2 = 189.98 - 45.54 = 144.44 \text{ VAR}$$

$$2. \theta_1 = 41.40 \therefore Q_1 = 166.98, \theta_2 = 18.19$$

$$\therefore Q_2 = 78.43$$

$$\text{Hence } Q = 166.98 - 78.43 = 88.55 \text{ VAR}$$

$$3. \theta_1 = 40.53 \therefore Q_1 = 571.12, \theta_2 = 18.19$$

$$\therefore Q_2 = 144.14$$

$$\text{Hence } Q = 571.12 - 144.14 = 426.98 \text{ VAR}$$

$$4. \theta_1 = 44.76 \therefore Q_1 = 625.66, \theta_2 = 18.19$$

$$\therefore Q_2 = 176.84$$

$$\text{Hence } Q = 625.66 - 176.84 = 448.82 \text{ VAR}$$



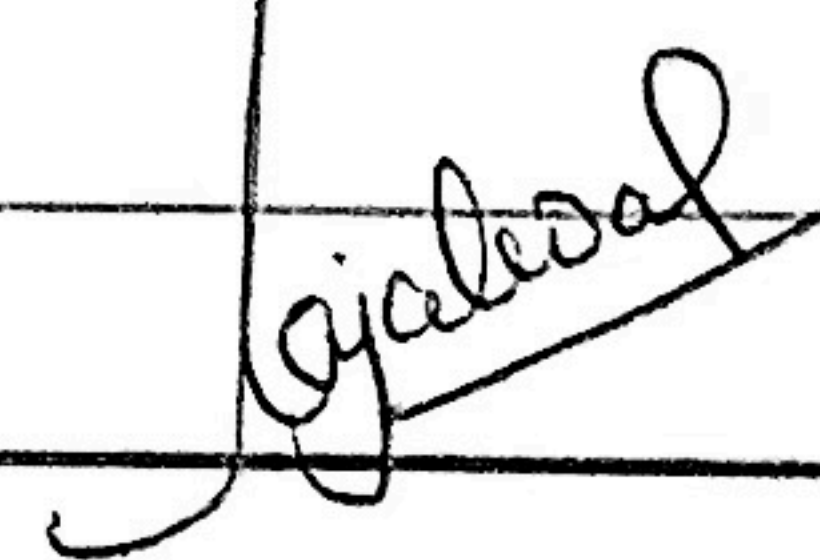
## OBSERVATION TABLE :

SL.	VOLTAGE	P.F.	$I_R$	$I_L$	$I_T$	
1.	230v	0.8	0.8	0.5	1.4	
2.	230v	0.75	0.8	1	1.1	
3.	220v	0.76	1.9	2.2	4	
4.	218v	0.71	2	2.6	4.1	

— WITHOUT COMPENSATION

SL.	VOLTAGE	P.F.	$I_R$	$I_L$	$I_T$	$I_C$
1.	230v	0.98	0.6	0.5	1	0.4
2.	230v	0.95	0.8	1	1.1	0.9
3.	220v	0.95	1.7	2.8	2.1	2.9
4.	218v	0.95	1.8	2.8	2.6	2.8

— WITH COMPENSATION





## Experiment - 7

AIM - To plot the IDMT characteristics of OC Relay.

APPARATUS REQUIRED - MC based OC relay Kit.

### CONNECTION PROCEDURE -

Connect current source output terminals C1A to C1 relay terminal & C2A to C2.

### PROCEDURE -

Switch on power and set relay parameters.

In relay set current value as 1A.

Switch on MCB and press START.

Apply some current by adjusting autotransformer

Now fault current of 2A is set.

Press STOP manually & then START.

The relay trips after some time & stop clock indicates relay trip time.

Repeat procedure.

### PRECAUTIONS -

Keep Auto-Transformer in minimum position and MCB when starting experiment.

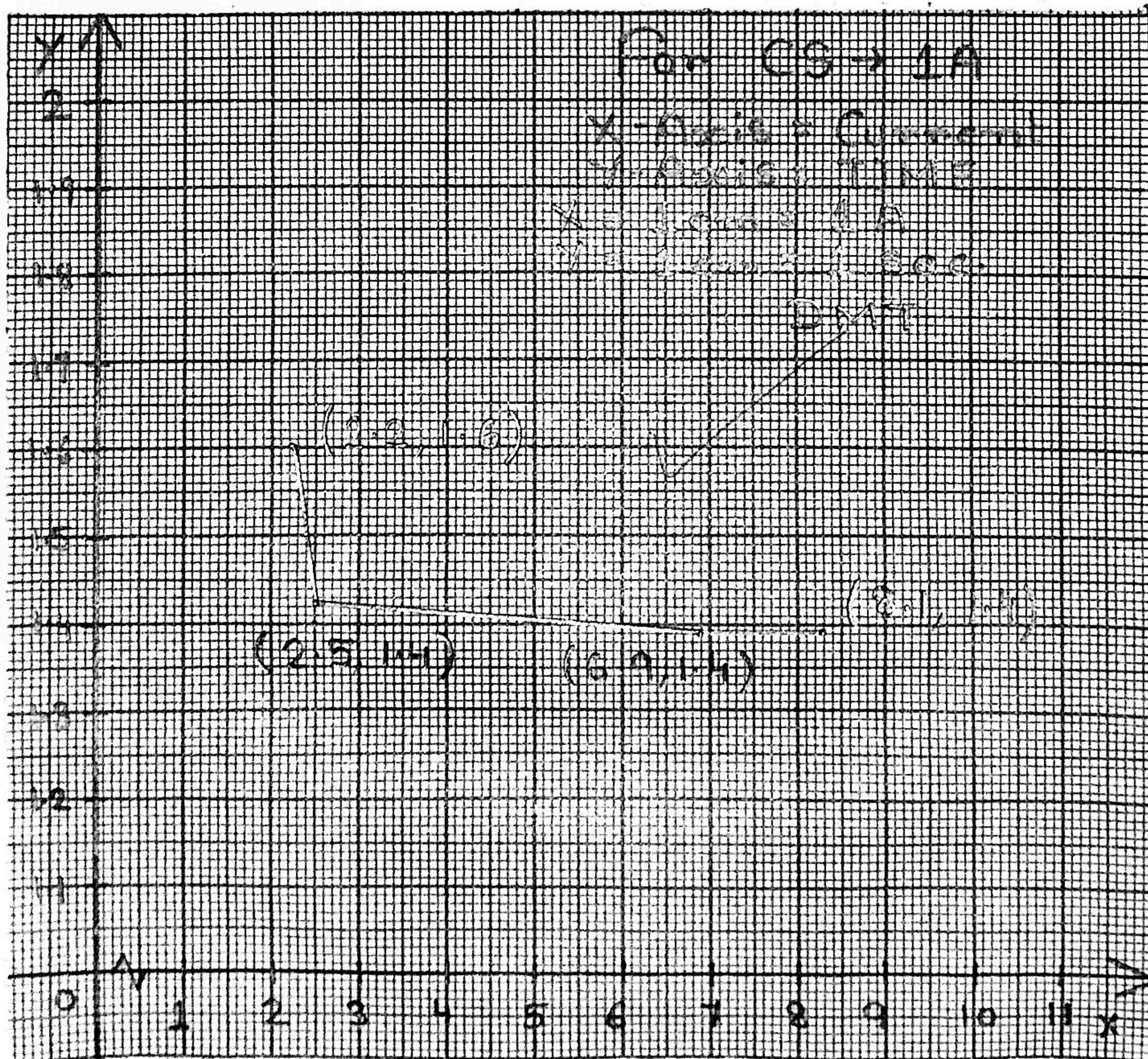


SL.	CURRENT	TIME
1.	2.25 A	1.6 s
2.	2.58 A	1.43 s
3.	6.93 A	1.39 s
4.	5.50 A	1.90 s
5.	8.18 A	1.40 s
6.	9.67 A	1.56 s
7.	10.74 A	1.50 s

DMT

FOR:

CURRENT SETTING  
= 1 A





## OBSERVATION TABLE-

SL.	CURRENT	TIME	
1.	2.13 A	9.98 s	IDMT FOR: CURRENT SETTING = 1A
2.	5.5 A	4.61 s	
3.	7.81 A	4.53 s	
4.	8.90 A	4.52 s	
5.	11.10 A	3.38 s	

SL.	CURRENT	TIME	
1.	3.35 A	16.03 s	FOR: CURRENT SETTING = 1.5 A
2.	2.98 A	17.44 s	
3.	3.51 A	9.45 s	
4.	4.88 A	6.98 s	

SL.	CURRENT	TIME	
1.	3.10 A	29.99 s	FOR: CURRENT SETTING = 2A
2.	3.16 A	17.41 s	
3.	3.44 A	13.10 s	
4.	4.95 A	8.23 s	



## Experiment - 8

AIM - Measurement of ABCD constants of a transmission line using transmission line kit.

### APPARATUS

Transmission line model kit

Variac (0-250 v)

Ammeter (0-2.5 A/5 A)

Voltmeter (0-200 v AC)

AC Ammeter (0-10 A)

Connecting Wires

### OBJECTIVE -

Model 600 KM transmission line with nominal T and  $\pi$  model & perform open-circuit & short circuit test from both ends & calculate ABCD parameters.

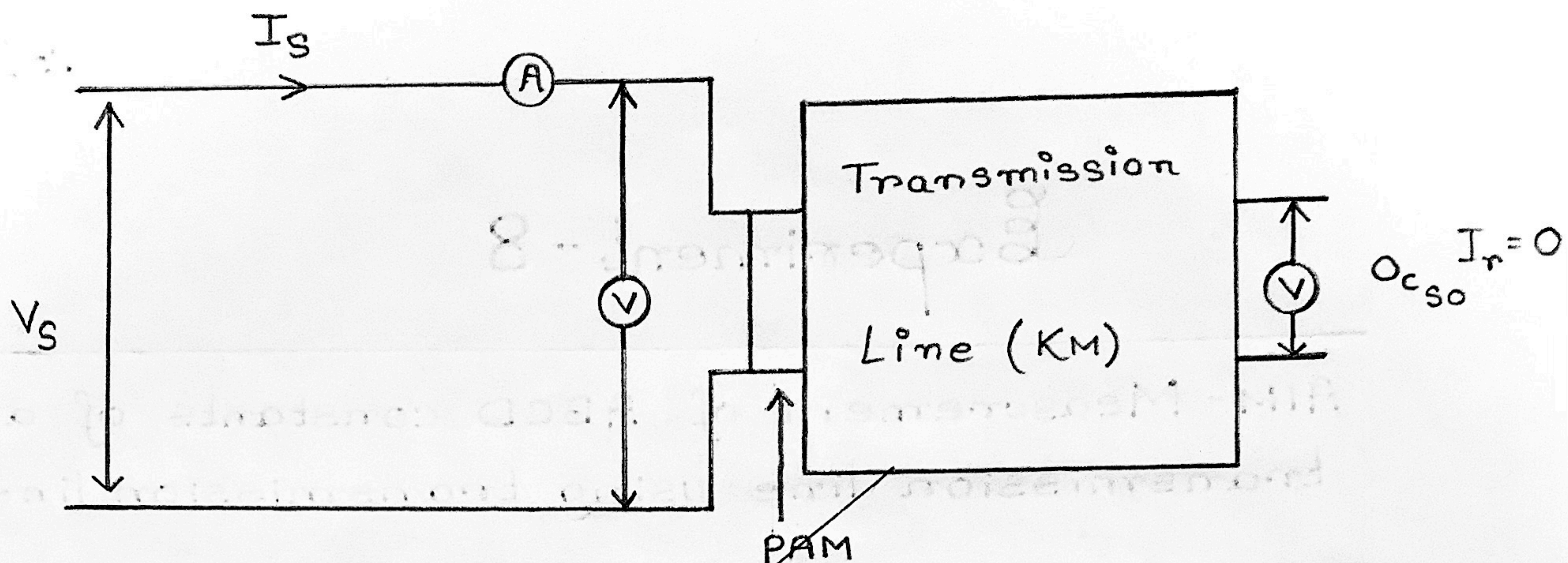
### THEORY -

In a transmission line sending & receiving end voltage is related by:

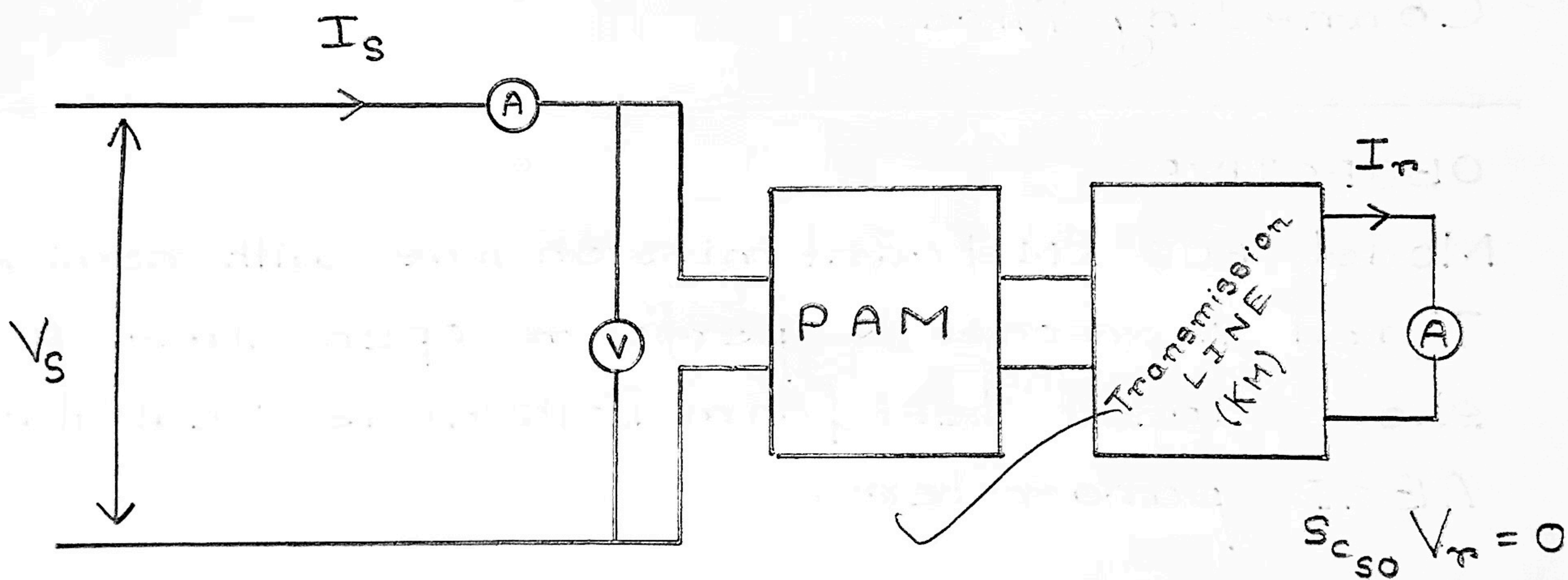
$$V_s = AV_r + BI_r$$

$$I_s = CV_r + DI_r$$





OPEN-CIRCUIT  
DIAGRAM



SHORT-CIRCUIT  
DIAGRAM



Similarly -

$$V_r = DV_s - BI_s = AV_s - BI_s$$

$$I_r = -CV_s + DI_s = -CV_s + AI_s$$

With  $AD - BC = 1$  &  $A = D$

The constants can be measured by an open circuit cum short circuit test at the end of lines.

For O.C. test on receiving end:

$$I_r = 0$$

$$V_{s0} = AV_{r0}$$

$$I_{s0} = CV_{r0} \text{ or } Z_{s0} = V_{s0}/I_{s0} = A/C$$

For S.C. test on receiving end:

$$V_r = 0$$

$$V_{sc} = BI_{rsc}$$

$$I_{sc} = DI_{rsc} \text{ or } Z_{sc} = V_{sc}/I_{sc} = B/D$$

If the supply is provided on receiving end -

$$V_r = DV_s + BI_s$$

$$-I_r = -CV_s + AI_s$$



Now,

For O.C. test on sending end:

$$I_s = 0$$

$$V_{r0} = AV_{s0}$$

$$-I_{r0} = -CV_{s0} \text{ or } Z_{r0} = D/C$$

For S.C. test on sending end:

$$V_s = 0$$

$$V_{rc} = BI_{sc}$$

$$I_{rc} = DI_{sc} \text{ or } Z_{sc} = B/A$$

For ABCD parameters:

$$Z_{r0} - Z_{rc} = D/C - B/A = AD - BC / AC = 1/AC$$

$$Z_{s0} / (Z_{r0} - Z_{rc}) = A/C \times 1 / (1/AC) = A^2$$

$$\text{or, } A = \sqrt{\frac{Z_{s0}}{Z_{r0} - Z_{rc}}} = D$$

$$B = AZ_{rc} \text{ \& } C = A/Z_{s0}$$



## PROCEDURE:

1. Connect the units in either T or  $\pi$  model.
2. Connect source 'S' to point A.
3. Switch 'ON' supply.
4. Gradually increase voltage until 0 v.
5. Perform SC/OC test accordingly.

## OBSERVATION TABLE:

## SHORT CIRCUIT;

SL.	SE Volt.	SE Current	RE Volt.	RE Current
1.	30 v	2 A	0 v	0.9 A

## OPEN CIRCUIT;

SL.	SE Volt.	SE Current	RE Volt.	RE Current
1.	20 v	1.3 A	38 v	0 A

## CALCULATIONS:

$$V_s = AV_R + BI_R$$

$$I_s = CV_R + DI_R$$



For open circuit where  $I_R = 0$ ;

$$V_S = AV_R \Rightarrow A = V_S/V_R = 20/38 = 0.526$$

$$I_S = CV_R \Rightarrow C = I_S/V_R = 1.3/3.8 = 0.342$$

For short circuit where  $V_R = 0$ ;

$$V_S = BI_R \Rightarrow B = V_S/I_R = 30/0.9 = 33.333$$

$$I_S = DI_R \Rightarrow D = I_S/I_R = 2/0.9 = 2.222$$

Hence :

$$A = 0.526 \Omega$$

$$B = 33.33 \Omega$$

$$C = 0.342 \Omega$$

$$D = 2.22 \Omega$$

ABCD parameters  
of Transmission  
Lines showing the  
Ferranti Effect.

RESULTS :

ABCD parameters were obtained from data.



## Experiment - 9

AIM - To study the measurements of a differential protection of a transformer.

APPARATUS - Trainer Kit

### FORMULAS :

$I_1$  = Primary Current

$I_2$  = Secondary Current

$$\therefore I_d = I_1 - I_2$$

$$I_r = (I_1 + I_2) / 2$$

$$DF_1 = 0.4 \text{ pu}, i_k = 0.2 \text{ pu}, K_p = 1 \text{ pu}$$

$$DF_2 = 0.8 \text{ pu}, \text{Diff. HiSet} = 0$$

$$\text{CTR } \omega_1 = 2, \omega_2 = 1.12$$

$$\text{InRush} = 0, \text{OverExcitation (5f)} = 0$$

$$\text{Vector Group} = Yd_1$$

$$I_d \gg DF_1 \times I_r + (1 - DF_1/2) \times I_k$$

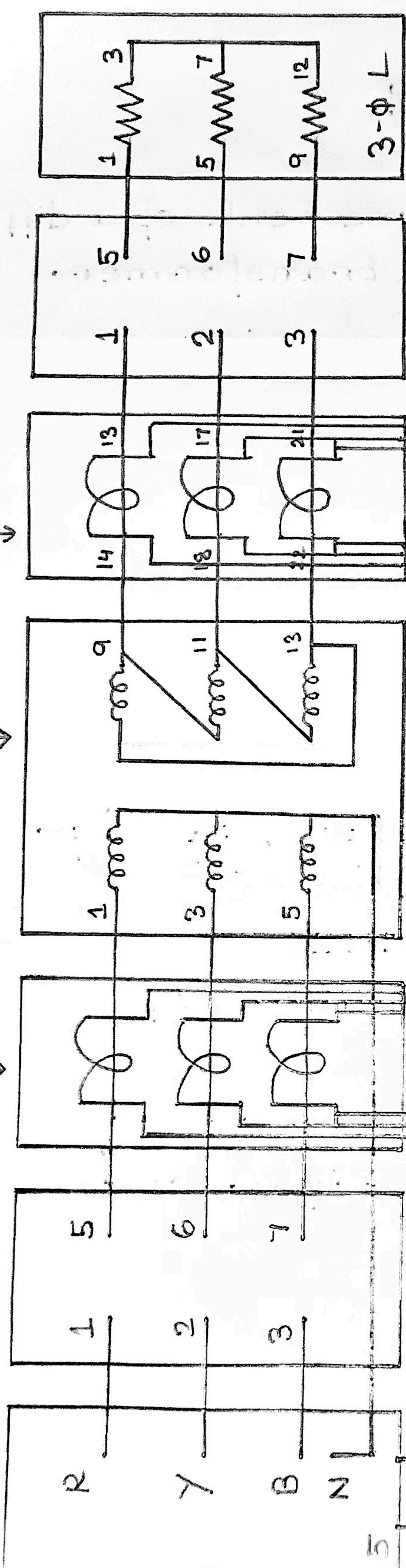


EMT-1

EMT 48

EMT 49

EMT 48



EMT 34/A

EMT-34/B

EMT - 16A  
1- $\phi$  AUX SUPPLY

DIFFERENTIAL  
RELAY

7 O/C MEASURE  
& TIMER  
EMT-39/2

FOR FAULT  
USE 14 & 16  
OF EMT 14/B

EMT-42A

CIRCUIT  
DIAGRAM



## PROCEDURE:

1. Make wiring sequence and observe table.
2. We are using 3- $\phi$  Numeric relay R, Y and B.
3. Keep load selection switch on EMT-42A at 125  $\Omega$  and on EMT-14B at OFF position.
4. Keep bypass switch on EMT-39 panel open.
5. Switch on AC supply by turning 4A MCB ON.
6. Press start push buttons PB1 on EMT 39 first & then on EMT 1 to switch on protection circuit.
7. If TRIP LED is on then press & hold reset push button for 3-5 sec otherwise ignore.
8. Now close bypass switch on EMT-39.
9. To create a fault on LL on primary side connect resistor on EMT 14B to transformer primary between R & Y phases, Keeping the resistance selection switch on EMT 14B OFF.
10. Put resistor selector switch on EMT 14B at 750  $\Omega$ . Note down values from display.

Now, again:

11. Press RESET button on relay panel.
12. To create a LN fault on primary side, connect resistor from EMT 14B between R & N of primary transformer EMT 49.
13. Press START push buttons on EMT 39 & EMT 1 to switch on protection circuit.



14. Put resistor selector switch on EMT 14B at  $750\ \Omega$  & then at  $300\ \Omega$  and note down.
15. Press RESET button & repeat for LL fault on secondary side and with resistor switch at  $750\ \Omega$ ,  $600\ \Omega$  &  $300\ \Omega$ . Note it.
16. Always note down resistance value from EMT 14B, current of primary ( $I_p$ ) and secondary ( $I_s$ ) from display panel.
17. Press RESET button & repeat for LL fault at primary, secondary by connecting a resistor from EMT 14B to secondary side of transformer EMT 49 between R-Y phase.
18. Push Start PB1 on EMT 39 & EMT 1.
19. Put resistor selector switch on EMT 14B at  $750\ \Omega$ ,  $600\ \Omega$ ,  $300\ \Omega$ ,  $212\ \Omega$  &  $162\ \Omega$ .
20. Note readings & press RESET.

### CONCLUSION:

From the above experiment it is observed that for any in-zone faults like LL, LG, LN whether primary or secondary the relay will trip.



## OBSERVATION TABLE:

SL	FAULT	Short R.	$I_p$	$I_s$	$I_d$
1.	L-L (primary)	750	52	21	31
2.	L-N (primary)	212	49	19	30
3.	L-L (secondary)	212	51	20	31

## CALCULATIONS:

$$1. I_1 = 52, I_2 = 21, I_d = 31, I_r = 0.36 \text{ pu}$$

$$= 0.52 \text{ pu} \quad = 0.21 \text{ pu} \quad = 0.31 \text{ pu}$$

$$DF_1 = 0.4 \text{ pu}, i_K = 0.2 \text{ pu}, K_p = 1 \text{ pu}$$

$$I_d \geq DF_1 \times I_r + (1 - DF_1/2) \times i_K$$

$$\therefore 0.31 \geq 0.30$$

$$2. I_1 = 0.49 \text{ pu}, I_2 = 0.19 \text{ pu}, I_d = 0.30 \text{ pu}, K_p = 1$$

$$\therefore I_d \geq DF_1 \times I_r + (1 - DF_1/2) \times i_K$$

$$\therefore 0.30 \geq 0.296$$

$$3. I_1 = 0.51 \text{ pu}, I_2 = 0.20 \text{ pu}, I_d = 0.31 \text{ pu}$$

$$\therefore I_d \geq DF_1 \times I_r + (1 - DF_1/2) \times i_K$$

$$\therefore 0.31 \geq 0.3$$